## Symmetrische Rollungen mit sphärischen Punktbahnen Symmetric Rollings with Spherical Trajectories

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39. Fortbildungstagung für Geometrie, Strobl, 8.-10. November 2018

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## **Overview**

- 1. Symmetric Rolling Motion
- 2. Basics on Hexapods and Self-Motions
- 3. Known Symmetric Rollings with Spherical Paths
- 4. Problem Formulation using Study Parameters
- 5. Duporcq Hexapod

Presented results are published in (and references are given with respect to):

G. NAWRATIL: Hexapods with plane-symmetric self-motions. In special issue Kinematics and Robot Design (R. Di Gregorio ed.), Robotics 7(2) #27 (2018)

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#### **1. Planar Symmetric Rolling**

During the constrained motion of a planar mechanism the instantaneous pole P traces the so-called fixed/moving polode in the fixed/moving system.

It is well known that this motion can also be generated by the rolling of the moving polode  $\varphi$  along the fixed polode  $\varphi_0$  without sliding.

If the polodes are symmetric with respect to the pole tangent t, then the motion is called *planar symmetric rolling*.



#### **1. Planar Symmetric Rolling**

In 1826, this motion was first studied by Quetelet [1], who pointed out that:

The path x of a point X under this special planar motion can be generated by the reflexion of a point  $X_0$  of the fixed system on each tangent of  $\varphi_0$ .

This can also be reformulated as follows: x can be obtained by a central dilation with center  $X_0$  and scale factor 2 (i.e., central doubling) of  $X_0$ 's pedal-curve f with respect to  $\varphi_0$ .



## **1. Spherical Symmetric Rolling**

The spherical counterpart of this motion is called *spherical symmetric rolling* and was extensively studied by Tölke [2].

The spherical version of the above given characterization also holds true for the spherical symmetric rolling.

From another perspective, a planar/spherical symmetric rolling is generated by reflecting the fixed system in a 1-parametric continuous set of lines/great circles.



The latter point of view is of importance for the spatial generalization of symmetric rollings, which can be done in multiple ways:

1. Darboux [5] noted a 2-parametric spatial motion, which is generated by the rolling of a moving surface  $\Phi$  on an indirect congruent fixed surface  $\Phi_0$ .

It also holds that the path-surface of a point X can be generated by the reflexion of a point  $X_0$  of the fixed system on each tangent-plane of  $\Phi_0$ ; i.e. the path-surface can be obtained by a central doubling of  $X_0$ 's pedal-surface with respect to  $\Phi_0$ 's tangent-planes.



2. Krames [6] considered line-symmetric motions as the 1-parametric spatial analogue. These motions are obtained by reflecting the moving system in a 1-parametric set of lines forming the so-called *basic surface*  $\Gamma$ .

The path x of a point X under a linesymmetric motion can be generated by the reflexion of a point  $X_0$  on each generator g of  $\Gamma$ ; i.e. x can be obtained by a central doubling of  $X_0$ 's pedalcurve f with respect to  $\Gamma$ 's rulings.



However, it should be pointed out that  $\Gamma$  differs from the fixed axode  $\Phi_0$ , which is generated by  $\Gamma$ 's central tangents (i.e. common normals of infinitesimal neighboring lines of  $\Gamma$ ).

 $\Phi_0$  and the moving axode  $\Phi$  are at each time instant symmetric with respect to the axis p of the instantaneous screw, which is in general not an instantaneous rotation.



3. It is astonishing that neither Tölke [2] nor Krames [6] mentioned the more apparent generalization by reflecting the fixed system in a 1-parametric continuous set of planes.

Less attention was paid to these socalled *plane-symmetric motions* in the literature until now. The basic properties of this motion type were reported by Bottema and Roth [8].



## **1. Plane-Symmetric Motion**

Given is a 1-parametric continuous set of planes  $\tau(t)$  with time t. By reflecting the fixed frame  $\mathfrak{F}_0$  on the plane  $\tau(t)$ , we obtain the pose  $\mathfrak{F}_0^t$ .

Two infinitesimal neighboring poses  $\mathfrak{F}_0^t$ and  $\mathfrak{F}_0^{t+\Delta t}$  can be transformed into each other by a reflexion on  $\tau(t)$  followed by a further reflexion on  $\tau(t + \Delta t)$ .

This is a pure rotation about the line p of intersection of  $\tau(t)$  and  $\tau(t + \Delta t)$ .



## **1. Plane-Symmetric Motion**

The axis p of this instantaneous rotation is a torsal ruling of the surface enveloped by the given 1-parametric set of planes.

Therefore the fixed axode  $\Phi_0$  is a developable surface and the corresponding moving axode  $\Phi$  is obtained by reflecting  $\Phi_0$  in  $\Phi_0$ 's tangent-plane  $\tau$  along p.

The path x of a point X under a planesymmetric motion can be generated by the reflexion of a point  $X_0$  on each tangent-plane  $\tau$  of  $\Phi_0$ 



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## **1. Plane-Symmetric Motion**

This can also be reformulated as follows: x can be obtained by a central doubling of X<sub>0</sub>'s pedal-curve f with respect to  $\Phi$ 's tangent-planes.

Due to these properties, the planesymmetric motion is the straightforward spatial counterpart of the planar/spherical symmetric rolling.

Therefore the plane-symmetric motion is also called *spatial symmetric rolling*.



A hexapod consists of a moving platform  $\Sigma$ and the fixed base  $\Sigma_0$ , which are linked with six legs anchored via spherical joints.

The geometry of a hexapod is given by the six base anchor points  $M_i \in \Sigma_0$  and by the six platform points  $m_i \in \Sigma$ .

For fixed leg lengths a hexapod is in general rigid. But, in some particular cases the hexapod can perform an *n*-parametric motion (n > 0), which is called *self-motion*.



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All self-motions are solutions to the problem posed by the French Academy of Science for the *Prix Vaillant* (1904), also known as

**Borel–Bricard problem** (still unsolved) Determine and study all displacements of a rigid body in which distinct points of the body move on spherical paths.

Clearly, in each pose of a self-motion the hexapod has to be *infinitesimal flexible*.



A hexapod is *singular* (*infinitesimal flexible*, *shaky*), if and only if, the carrier lines of the six legs belong to a linear line complex.

A hexapod is called *architecturally singular* if the six legs belong in each relative pose of the platform with respect to the base to a linear line complex.

These special solutions to the Borel–Bricard problem are already well studied (review on this topic is given in [15]).



The approaches for the determination of non-architecturally singular hexapods recorded in the literature, can roughly be divided into the following two groups:

- 1. Assumptions on the geometry of the platform and base; e.g.,
  - ★ linear mapping between platform and base [16-22],
  - ★ symmetry properties of platform and base [20-24] (cf. Figure),
  - \* special topology (e.g. octahedral structure [25]),

or a combination of these assumptions (e.g. [20–22]).



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- 2. Assumptions on the self-motion; e.g.,
  - \* line-symmetric self-motion [9],
  - \* type II Darboux–Mannheim selfmotion [26],
  - \* Schoenflies self-motion [27],
  - \* translational self-motion [28],
  - \* self-motion of maximal degree [29] (cf. Figure),

or more generally characterizations like *linear relations between direction cosines* [30–33].  $M_6$   $M_5$   $M_4$   $M_3$   $M_2$   $M_1$   $M_2$   $M_1$   $M_2$   $M_1$   $M_2$   $M_2$   $M_1$   $M_2$   $M_2$   $M_1$   $M_2$   $M_2$   $M_2$   $M_2$   $M_3$   $M_2$   $M_2$   $M_3$   $M_2$   $M_2$   $M_3$   $M_2$   $M_3$   $M_2$   $M_2$   $M_3$   $M_3$   $M_2$   $M_3$   $M_3$ 

These assumptions are done to reduce the complexity of the problem, as one has to deal with 29 design parameters and 6 degrees of freedom.



## 3. Planar Symmetric Rollings with Circular Paths

All planar symmetric rollings with points running on circular paths were determined by Bereis [3].

a) The polodes are ellipses and the focals of the moving ellipse are running on circles.

This motion can be realized by a twin-crank mechanisms with non-counter-rotating cranks.



## 3. Planar Symmetric Rollings with Circular Paths

b) The polodes are hyperbolas and the focals of the moving hyperbola are running on circles.

This motion can be realized by a twin-crank mechanisms with counter-rotating cranks.



## **3. Spherical Symmetric Rollings with Circular Paths**

Spherical symmetric rollings with circular paths are generated by spherical isograms, which are studied in more detail in [34].

The moving and fixed polode are spherical conics. As on the sphere points can be replaced by their antipodes, it can be shown [35] that every spherical conic can be interpreted as a spherical ellipse.



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# **3. Spherical Symmetric Rollings with Circular Paths**



If we replace A and A<sub>0</sub> by their antipodal points  $\overline{A}$  and  $\overline{A_0}$ , respectively, and look on the sphere from the right side, then we get the figure illustrated on the right.

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# 3. Resulting Hexapods with Symmetric Self-Motions



The axodes of the self-motions are cylinders (left) and cones (right), respectively, but only the planar/spherical directrices of these singular quadrics are illustrated.

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## **3. Hexapods with Trivial Symmetric Self-Motions**

Clearly, a pure rotation is a symmetric rolling where every point of the moving system traces a circle. This trivial case (butterfly self-motion) arises for:

- $\star$  M<sub>1</sub>,... M<sub>i</sub> are collinear and
- $\star$  m<sub>i+1</sub>,..., m<sub>6</sub> are collinear with  $1 \leq i \leq 5$ .

If the collinearity is replaced by coincidence then there exists even a 2dimensional spherical self-motion.





## 3. Known Self-Motions are Line-Symmetric

If we embed the planar/spherical symmetric rollings into the group SE(3) of Euclidean displacements, then they can also be seen as line-symmetric motions.

Therefore, all the self-motions of the hexapods given so far are symmetric rollings and line-symmetric motions at the same time.

This raises also the question of whether self-motions exist, which are symmetric rollings but not line-symmetric.

An answer can be obtained by formulating the problem in terms of algebraic geometry by means of Study parameters  $(e_0 : e_1 : e_2 : e_3 : f_0 : f_1 : f_2 : f_3)$ .



#### 4. Problem Formulation using Study Parameters

There is a bijection between SE(3) and real points of the 7-dimensional Study parameter space  $P^7$ , which are located on the so-called Study quadric  $\Psi$ :  $\sum_{i=0}^{3} e_i f_i = 0$ sliced along the 3-dimensional subspace  $e_0 = e_1 = e_2 = e_3 = 0$ .

For  $e_0^2 + e_1^2 + e_2^2 + e_3^2 = 1$  the translation vector  $\mathbf{t} := (t_1, t_2, t_3)^T$  and the rotation matrix  $\mathbf{R} := (r_{ij})$  of the corresponding Euclidean displacement  $\mathbf{x} \mapsto \mathbf{R}\mathbf{x} + \mathbf{t}$  are given by:

$$t_1 = 2(e_0f_1 - e_1f_0 + e_2f_3 - e_3f_2),$$
  

$$t_2 = 2(e_0f_2 - e_2f_0 + e_3f_1 - e_1f_3),$$
  

$$t_3 = 2(e_0f_3 - e_3f_0 + e_1f_2 - e_2f_1),$$

$$\mathbf{R} = \begin{pmatrix} e_0^2 + e_1^2 - e_2^2 - e_3^2 & 2(e_1e_2 - e_0e_3) & 2(e_1e_3 + e_0e_2) \\ 2(e_1e_2 + e_0e_3) & e_0^2 - e_1^2 + e_2^2 - e_3^2 & 2(e_2e_3 - e_0e_1) \\ 2(e_1e_3 - e_0e_2) & 2(e_2e_3 + e_0e_1) & e_0^2 - e_1^2 - e_2^2 + e_3^2 \end{pmatrix}$$

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## 4. Problem Formulation using Study Parameters

The reflection on a plane is an orientation-reversing congruence transformation, which cannot be described directly by the Study parameters. Therefore, we follow the approach of Selig and Husty [7], which is as follows:

- We start with a reflexion on a fixed plane; say the xy-plane of the fixed frame  $\mathfrak{F}_0$ . By this plane-reflection of  $\mathfrak{F}_0$ , we obtain  $\overline{\mathfrak{F}}_0$ .
- Then we apply the reflexion on the plane  $\tau(t)$ , which finally yields the pose  $\overline{\mathfrak{F}}_0^t$ .

As the composition of two plane-reflexions is again a direct congruence transformation, we can describe the plane-symmetric motions in this way.

As a consequence plane-symmetric motions are given by  $e_3 = f_0 = f_1 = f_2 = 0$ ; i.e. this corresponds to a 3-dimensional generator space  $P^3$  of  $\Psi$ .

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#### 4. Symmetric Rollings with Spherical Paths

Due to the symmetry of the motion the following theorem holds:

**Theorem 2.** If a point A of the moving system traces a spherical path with center  $B_0$  during a symmetric rolling, then also the point B of the moving system has a spherical trajectory about the point  $A_0$ , where A and  $A_0$  as well as B and B<sub>0</sub> are the symmetric points of the moving and fixed system.

Due to this symmetric-leg replacement the set of base points and platform points are indirectly congruent.



## 4. Spatial Symmetric Rollings with Spherical Paths

The condition that the point  $m_i$  is located on a sphere centered in  $M_i$  is a quadratic homogeneous equation in the Study parameters according to Husty [36].

Therefore it corresponds to a quadric  $\Lambda_i$  in the 3-dimensional projective space  $P^3$  with homogenous coordinates  $(e_0 : e_1 : e_2 : f_3)$ .

Due to the symmetric-leg replacement, we only have to find spatial rolling motions where three points run on spheres. This means that the corresponding three quardrics  $\Lambda_1$ ,  $\Lambda_2$  and  $\Lambda_3$  of  $P^3$  have to have a curve in common, which can be a:

\* straight line \* conic section \* cubic curve \* quartic curve



A discussion of cases shows that there exists only one further hexapod with planesymmetric self-motions, which are neither planar nor spherical. This manipulator is the so-called *Duporcq hexapod*.



 $M_1, \ldots, M_6$  and  $m_1, \ldots, m_6$  be the vertices of two congruent complete quadrilaterals, which are labeled in a way that  $m_i$  is the opposite vertex of  $M_i$ .

It is well known [39] that the Duporcq hexapod is architecturally singular.



Due to Duporcq [38] this hexapod has a 2-parametric line-symmetric self-motion. There are four transition poses between this line-symmetric self-motion and the 1parametric plane-symmetric self-motion. All four branching singularities are totally flat configurations.





Recall that the sphere condition  $\Lambda_i$  is a homogenous quadratic equation in  $e_0, e_1, e_2, f_3$ .

We express  $f_3$  from the condition  $\Lambda_2 - \Lambda_1$ , which is linear in  $f_3$ .

Plugging the resulting expression into  $\Lambda_1$  implies a homogenous quartic equation  $\Upsilon$  in  $e_0, e_1, e_2$ , which represents the plane-symmetric self-motion.

The quartic  $\Upsilon$  is displayed under consideration of the normalization condition  $e_0^2+e_1^2+e_2^2=1.$ 



If ax + by + cz + d = 0 is the equation of the plane of symmetry, then its dual representation is given by the homogenous quadruplet  $(u_0 : u_1 : u_2 : u_3) =$ (d : a : b : c) according to [11].

The fixed axode corresponds to an algebraic curve of degree 4 in the dual representation, which results from the intersection of two cylinders of degree 4 and one quadratic cylinder.

This curve can be parametrized (two branches).



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Trajectories of the platform points during the planesymmetric self-motion between the totally flat transition poses 1 and 2.

In the lower left corner a blow up of the fixed axode  $\Phi_0$  (including its line of regression c) is displayed.



Trajectories of the platform points during the planesymmetric self-motion between the totally flat transition poses 3 and 4.

In the upper right corner a blow up of the fixed axode  $\Phi_0$  (including its line of regression c) is displayed.





The Duporcq manipulator also has a 1-parametric translational selfmotion (circular translation).

There are two transition poses between this translational self-motion and the 2-parametric line-symmetric self-motion. Again both branching singularities are totally flat configurations.



This circular translation can also be seen as a point-symmetric motion, where the corresponding curve (halfcircle) is illustrated in red.

Note that there is no branching singularity between plane-symmetric self-motions and point-symmetric self-motions.



# Conclusion

Summed up one can say, that the Duporcq hexapod is a twofold kinematotropic mechanism, as there are branching singularities between the 2-dimensional line-symmetric self-motion and the 1-dimensional

- point-symmetric self-motion,
- plane-symmetric self-motion.

Due to its kinematotropic behavior and its total flat branching singularities the Duporcq manipulator is possibly of interest for the design of deployable structures.

#### Acknowledgements

The research was supported by Grant No. P 24927-N25 of the Austrian Science Fund FWF within the project "Stewart Gough Platforms with Self-Motions".

