

# Kokotsakis meshes and flexible quad meshes

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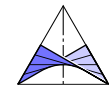


# Outline

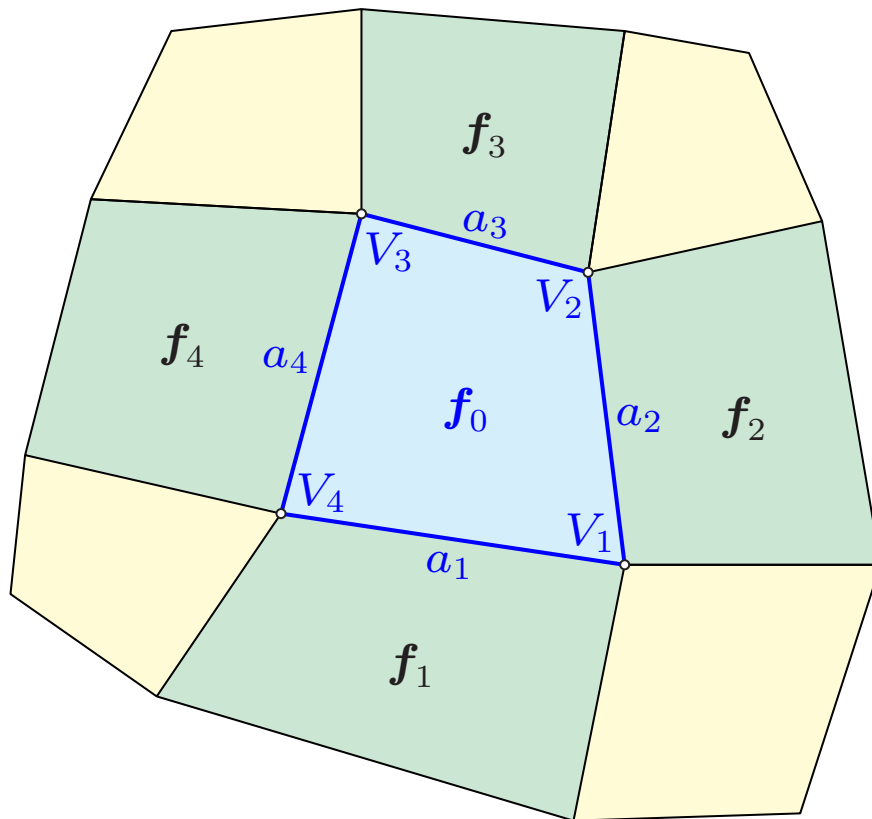
1. Flexible Kokotsakis meshes
2. Kokotsakis' flexible tessellation
3. Rigidity of a quadrangular cylinder tiling

**Funding source:** Grant No. I 408-N13 of the Austrian Science Fund FWF within the project "*Flexible polyhedra and frameworks in different spaces*", an internat. cooperation between FWF and RFBR (Russian Foundation for Basic Research)

**Acknowledgement:** Georg Nawratil, TU Wien



# 1. Flexible Kokotsakis meshes



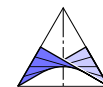
Special case  $n = 4$

A **Kokotsakis mesh** is a polyhedral structure consisting of an  $n$ -sided central polygon  $f_0$  surrounded by a belt of polygons.

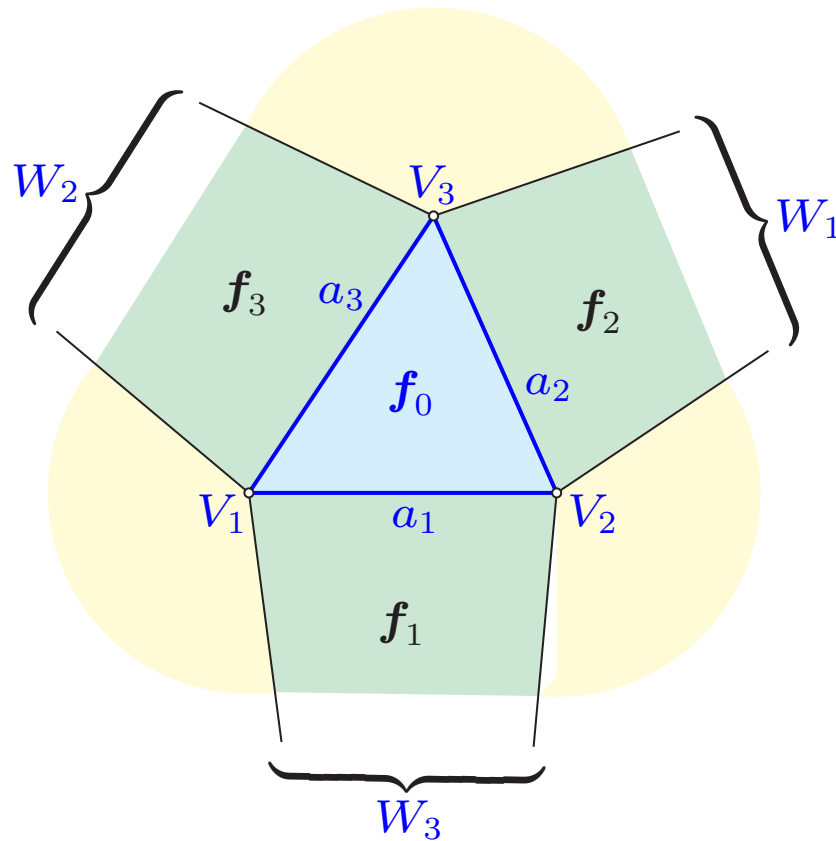
Each side  $a_i$ ,  $i = 1, \dots, n$ , of  $f_0$  is shared by a polygon  $f_i$ . At each vertex  $V_i$  of  $f_0$  four faces are meeting.

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Each face is a **rigid body**; only the dihedral angles can vary ('rigid origami'). Can it be continuously flexible?



# 1. Flexible Kokotsakis meshes

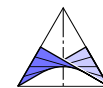


Special case:  $n = 3$

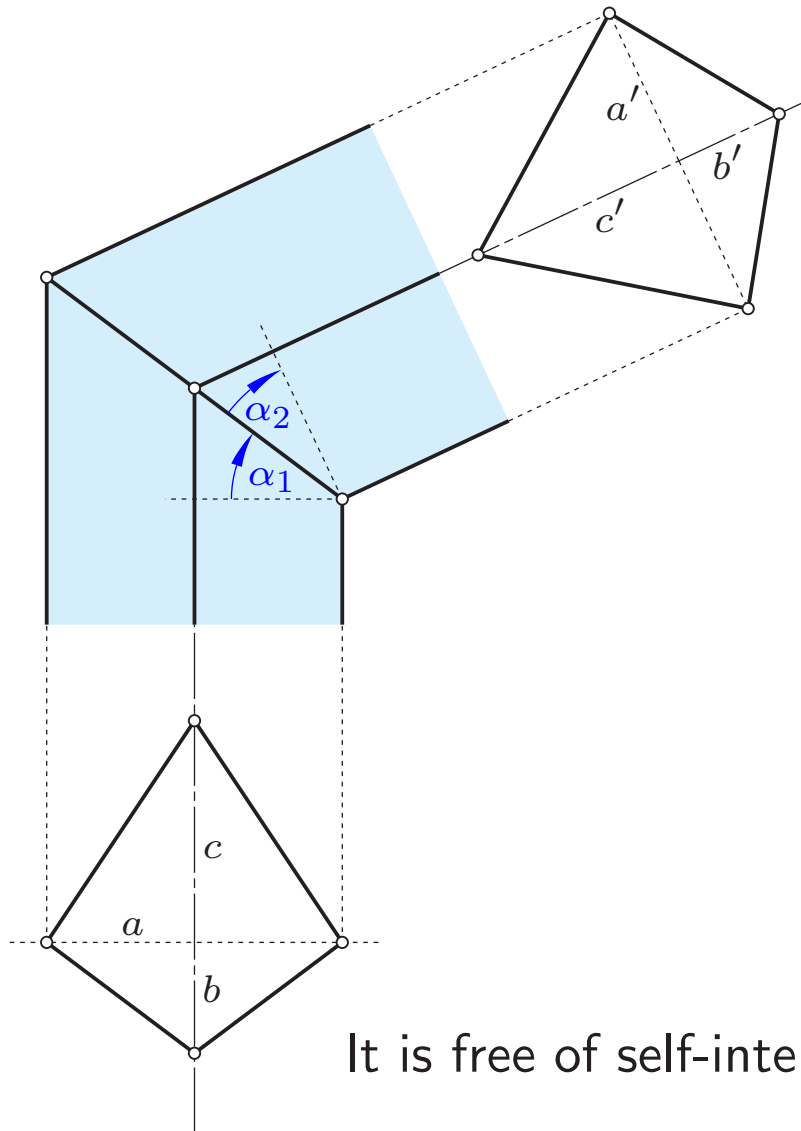
A Kokotsakis mesh for  $n = 4$  is also called **Neunflach** [German] (**nine-flat**) (KOKOTSAKIS 1931, SAUER 1932)

For  $n = 3$  the Kokotsakis mesh is equivalent to an **octahedron** with  $V_1V_2V_3$  and  $W_1W_2W_3$  as opposite triangular faces.

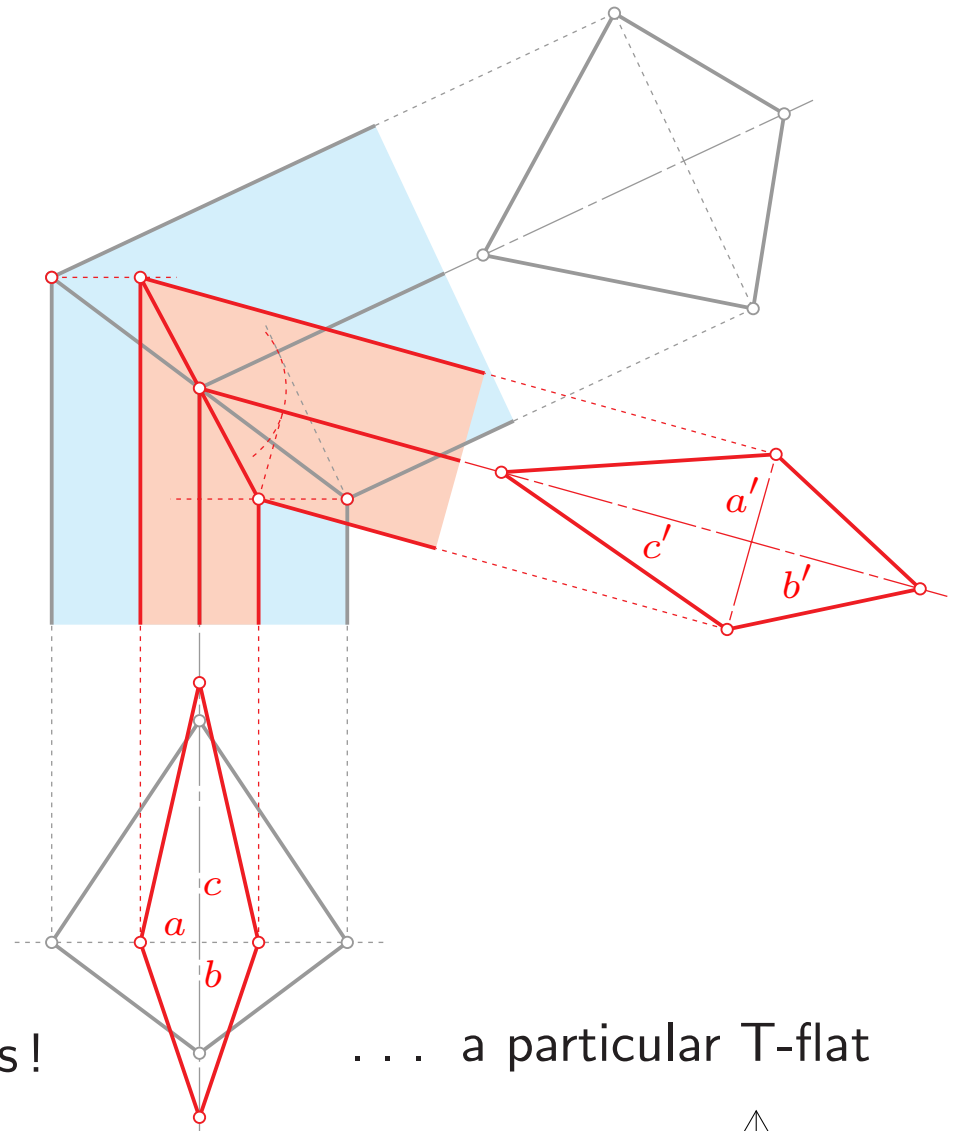
This offers an alternative approach to **R. BRICARD's flexible octahedra**.



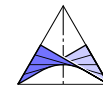
G. Nawratil: There is exactly **one** flexible octahedron with **vertices at infinity**.



It is free of self-intersections!



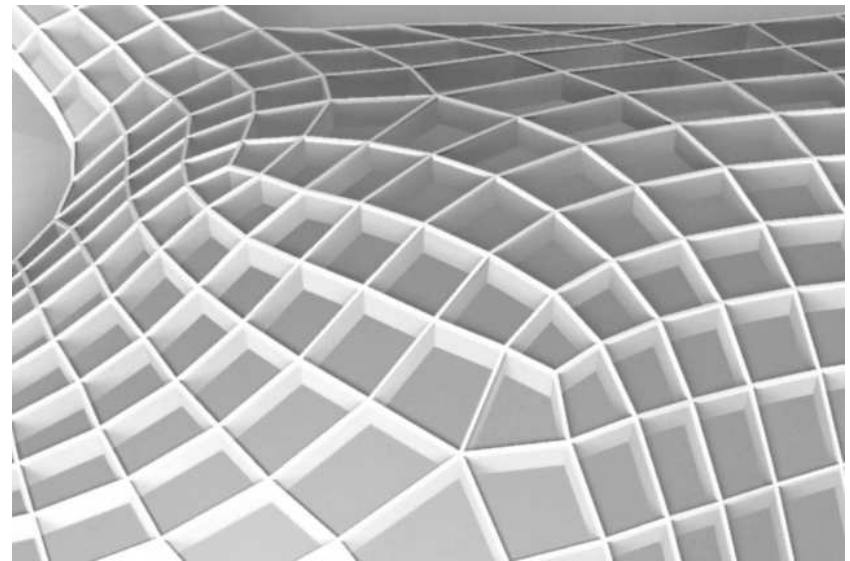
... a particular T-flat



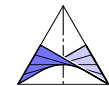
# 1. Flexible Kokotsakis meshes

In *discrete differential geometry* there is an interest on polyhedral structures composed of quadrilaterals (**quadrilateral surfaces**).

If all quadrilaterals are **planar**, they form a *discrete conjugate net* = **quad mesh**.



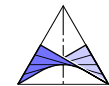
H. POTTMANN, Y. LIU, J. WALLNER,  
A. BOBENKO, W. WANG:  
*Geometry of Multi-layer Freeform  
Structures for Architecture.* ACM Trans.  
Graphics **26** (3) (2007), SIGGRAPH 2007



# 1. Flexible Kokotsakis meshes



In 'Freeform Architecture' most of the surfaces are designed as *polyhedral surfaces* — like the [Capital Gate in Dubai](#) (height = 160 m, inclination  $18^\circ$ )  
Steel construction: Wagner Biro, Austria



# 1. Flexible Kokotsakis meshes

**Theorem:** [BOBENKO, HOFFMANN, SCHIEF 2008]

*A discrete conjugate net in general position is **continuously flexible**  $\iff$  all its  $3 \times 3$  complexes are **continuously flexible**.*

The classification of all flexible Kokotsakis meshes ( $n = 4$ ) has **recently** be finished:

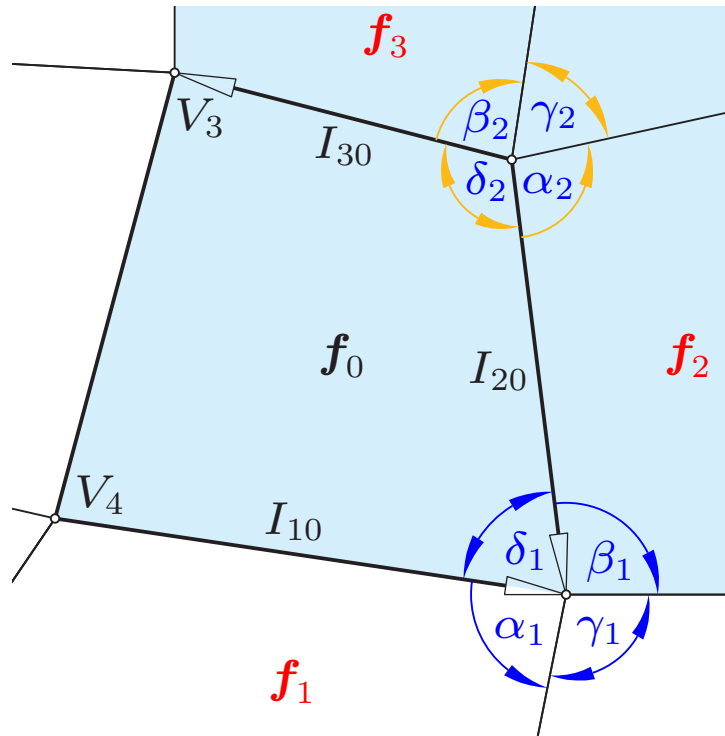
**Ivan IZMESTIEV:** *Classification of flexible Kokotsakis polyhedra with quadrangular base*, preprint, 74 p., May **2013**

A historical model of a flexible Kokotsakis meshes:

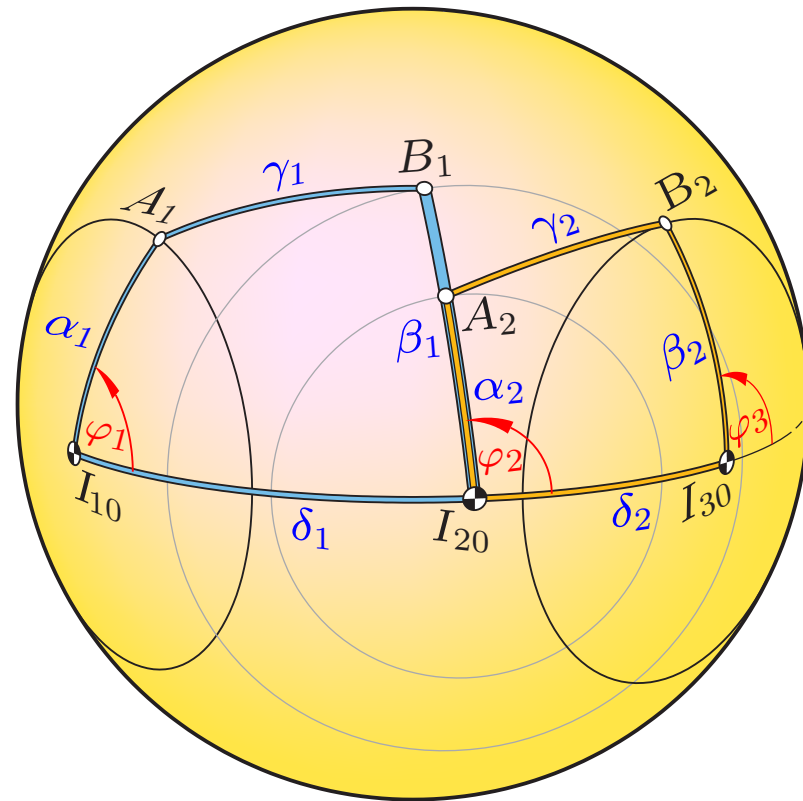




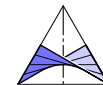
# 1. Flexible Kokotsakis meshes



Transmission from  $f_1$  to  $f_3$   
via  $V_1$  and  $V_2$ .



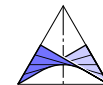
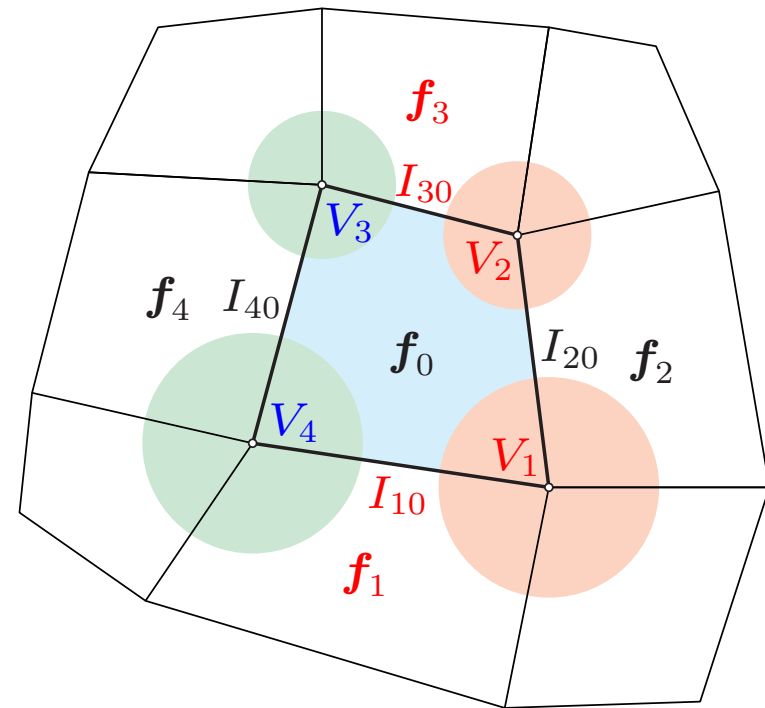
The composition of two spherical four-bars.



# 1. Flexible Kokotsakis meshes

Continuous flexibility of a Kokotsakis mesh for  $n = 4$  means:

The transmission from  $f_1$  to  $f_3$  can be decomposed in two different ways, via  $V_1$  and  $V_2$  – or via  $V_4$  and  $V_3$ .



# 1. Flexible Kokotsakis meshes

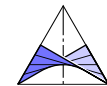
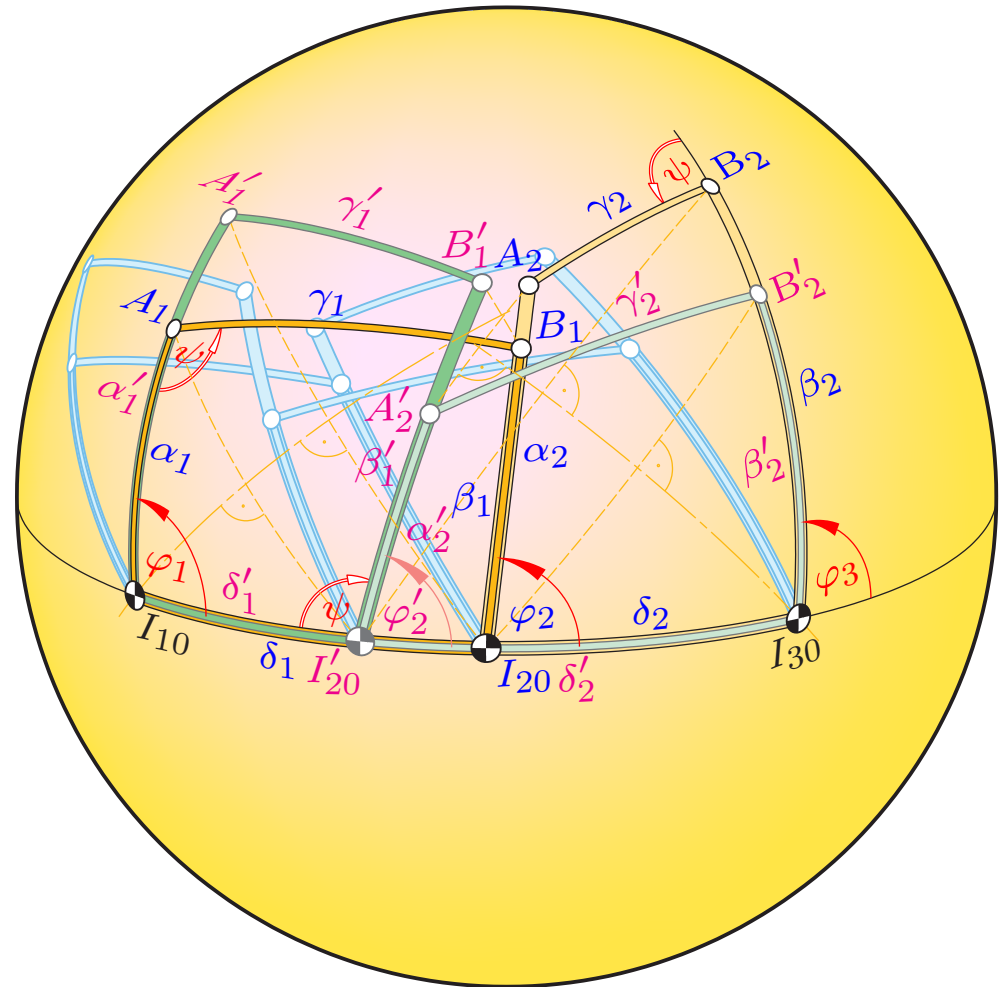
Conditions for one flexible case:

$$\alpha_1 + \beta_2 = \delta_1 + \delta_2$$

$$s\alpha_1 s\gamma_1 : s\beta_2 s\gamma_2 = s\beta_1 s\delta_1 : s\alpha_2 s\delta_2 = (c\beta_1 c\delta_1 - c\alpha_1 c\gamma_1) : (c\beta_2 c\gamma_2 - c\alpha_2 c\delta_2)$$

Right: The spherical image of this case with **two decompositions**.

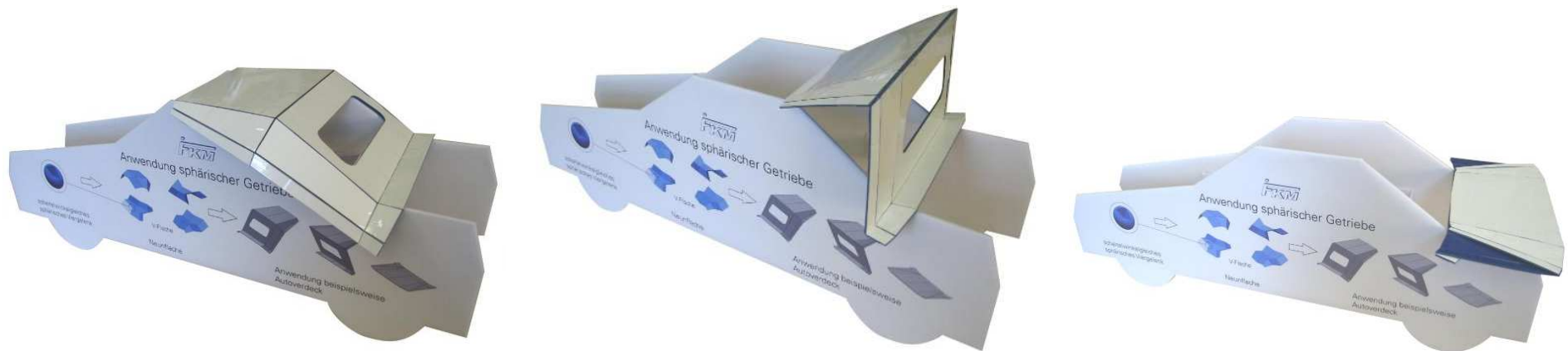
A second pose is shown in light-blue.



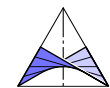
# 1. Flexible Kokotsakis meshes

Only in very particular cases we know something about the **geometry of the flexions** obtained during the self-motions of continuously flexible Kokotsakis meshes and quad meshes,

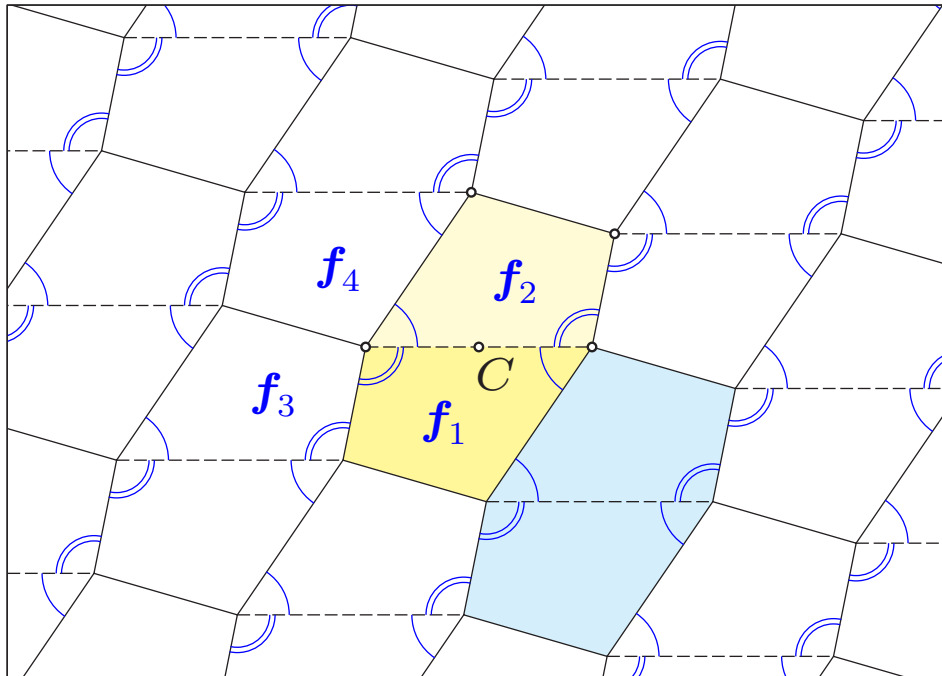
e.g., application of a **discrete Voss surface** in



Nadja Posselt: *Synthese von zwangläufig beweglichen 9-gliedrigen Vierecksflächen*, diploma thesis, TU Dresden 2010



## 2. Kokotsakis' flexible tessellation



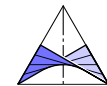
A. KOKOTSAKIS, 1932  
Athens

Any plane quadrangle is a tile for a **regular tessellation** of the plane (wallpaper group **p2**, generically).

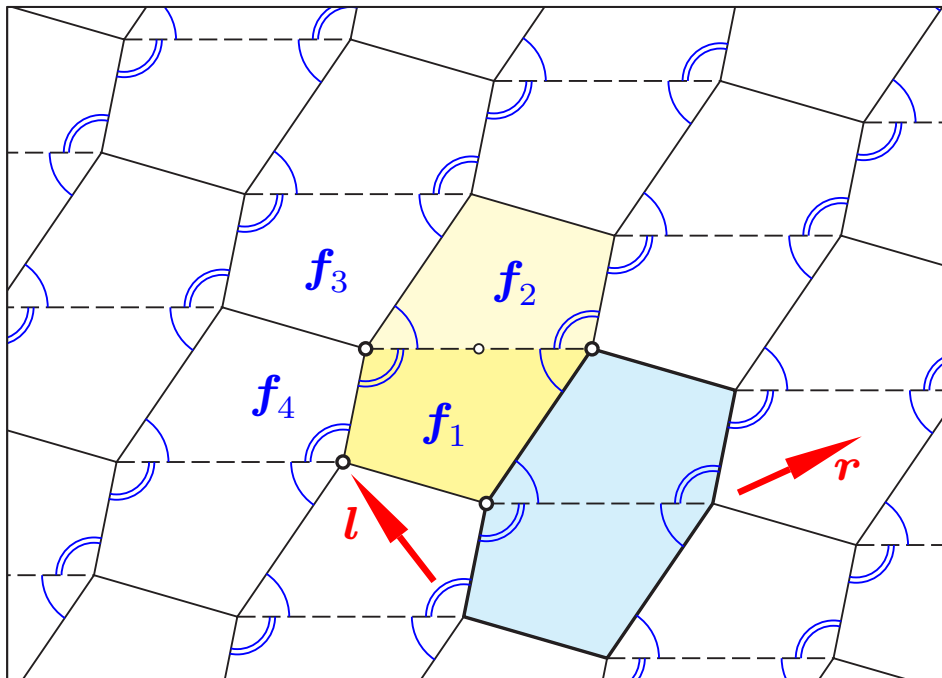
It is obtained by applying

- **iterated  $180^\circ$ -rotations** about the midpoints of the sides of an initial quadrangle or
- by applying **iterated translations** on a centrally symmetric **hexagon**.

For a convex  $f_1$  this polyhedral structure is continuously flexible.



## 2. Kokotsakis' flexible tessellation



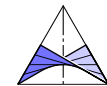
A. KOKOTSAKIS, 1932  
Athens

Any plane quadrangle is a tile for a **regular tessellation** of the plane.

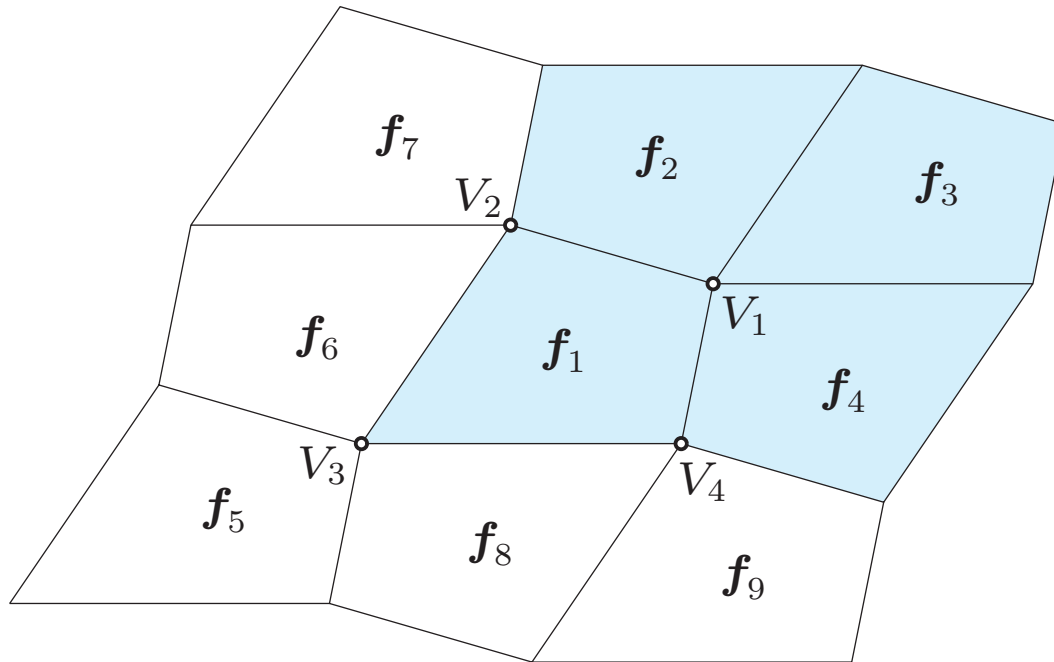
It is obtained by applying

- **iterated 180°-rotations** about the midpoints  $C$  of the sides of an initial **quadrangle** or
- by applying **iterated translations**  $l, r$  on a centrally symmetric hexagon.

For a **convex**  $f_1$  this polyhedral structure is **continuously flexible**.



## 2. Kokotsakis' flexible tessellation

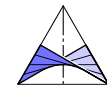


We pick out a  $3 \times 3$  complex from this tessellation. Why it is flexible?

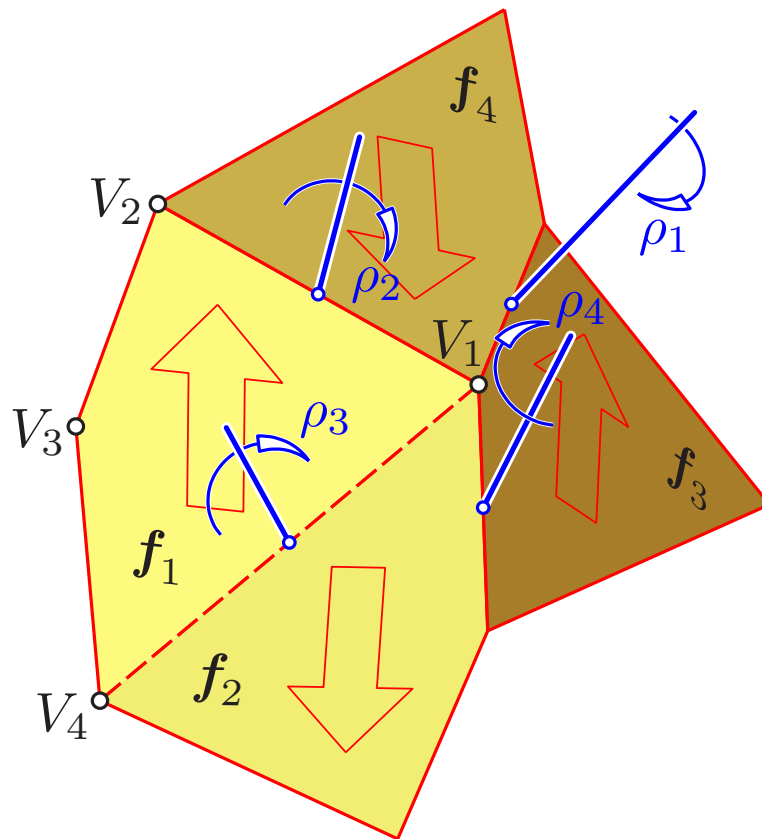
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We first focus on the four-sided pyramide with vertex  $V_1$ .

Due to the required **convexity** no interior angle is  $> \pi$ . Therefore this pyramide is continuously flexible.

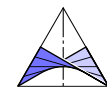


## 2. Kokotsakis' flexible tessellation



In each pose for any two neighbouring faces there is a  $180^\circ$ -rotation  $\rho_i$  which interchanges these two faces.

The **axis** is located in a bisector plane and passes through the midpoint of the common edge.



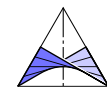
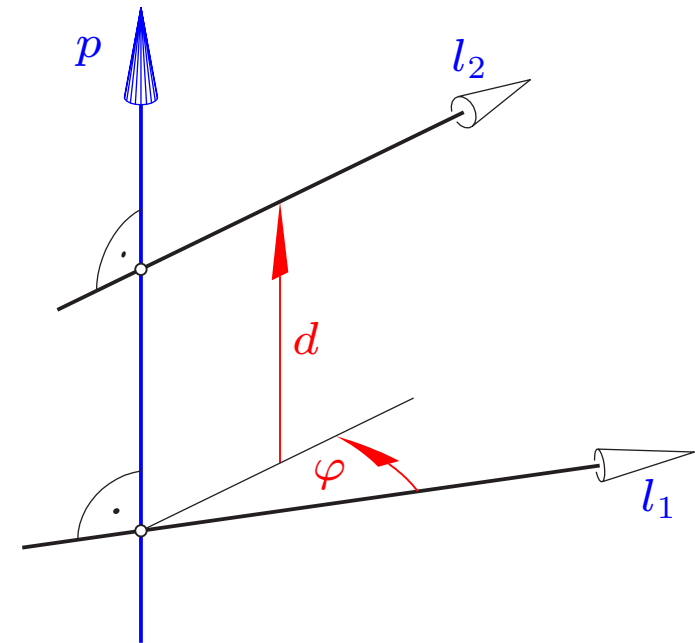


## 2. Kokotsakis' flexible tessellation

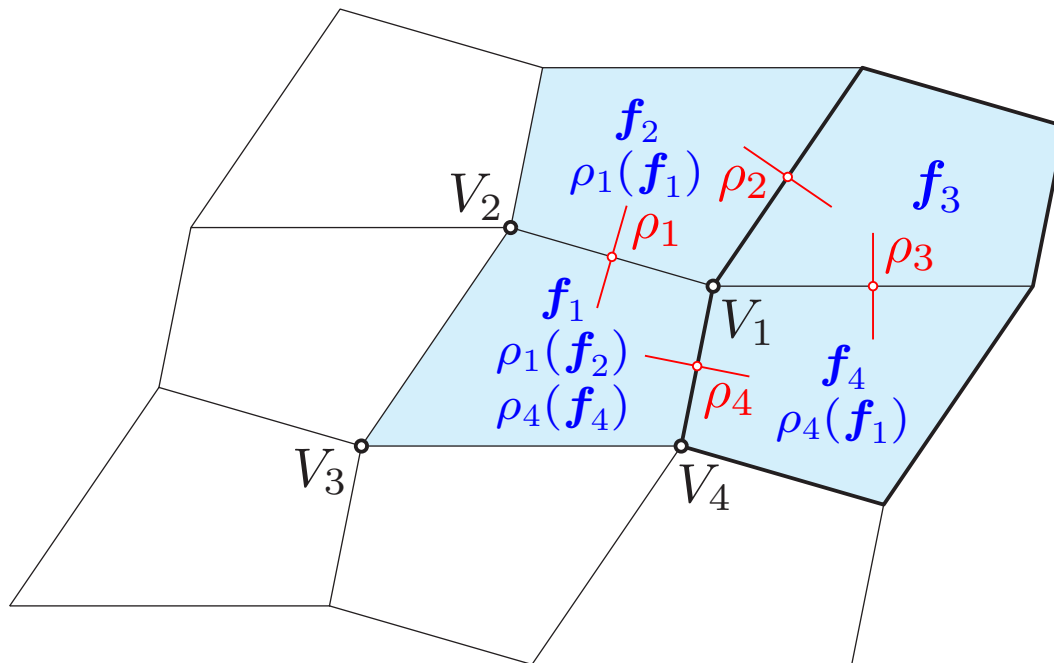
The **product** of any two  $180^\circ$ -rotations  $\rho_1, \rho_2$  about respective axes  $l_1$  and  $l_2$  is a **helical motion**  $\rho_2 \circ \rho_1$  about the common perpendicular  $p$ :

angle of rotation:  $2\varphi$

length of translation:  $2d$



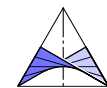
## 2. Kokotsakis' flexible tessellation



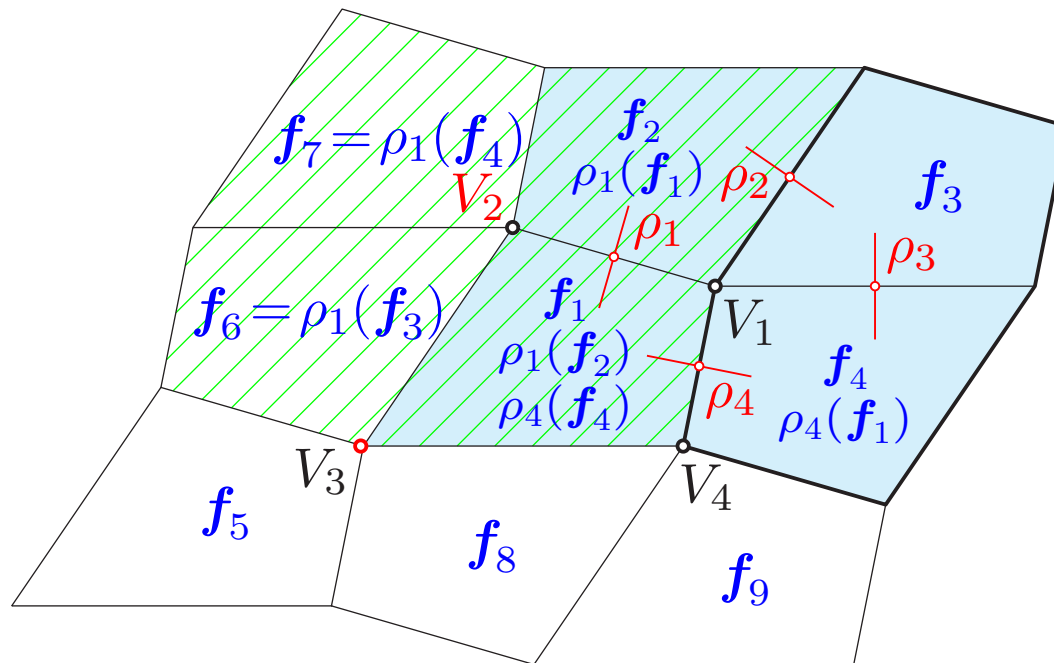
After applying all four  $180^\circ$ -rotations consecutively to the quadrangle  $f_1$ , this is mapped via  $f_2, f_3, f_4$  onto itself, hence

$$\rho_3 \circ \rho_4 = \rho_2 \circ \rho_1 .$$

$\implies$  the four axes have a **common perpendicular**  $p$ , and all vertices  $V_1, \dots, V_4$  are at the same distance from  $p$ .



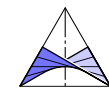
## 2. Kokotsakis' flexible tessellation



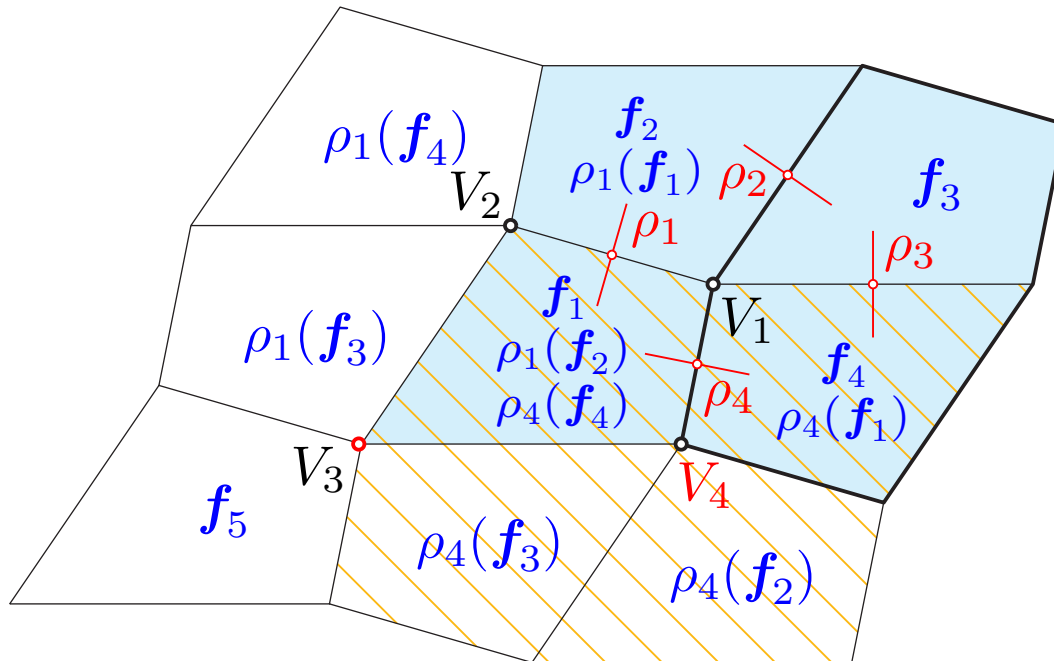
$\rho_1$  maps the pyramid with vertex  $V_1$  onto the pyramid with vertex  $V_2$ .

(There would also be a second possibility to continue the flexion of the  $2 \times 2$  mesh to  $f_6$  and  $f_7$ .)

There are two possibilities to continue the flexion onto the fourth pyramid with vertex  $V_3$ .



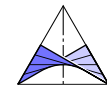
## 2. Kokotsakis' flexible tessellation



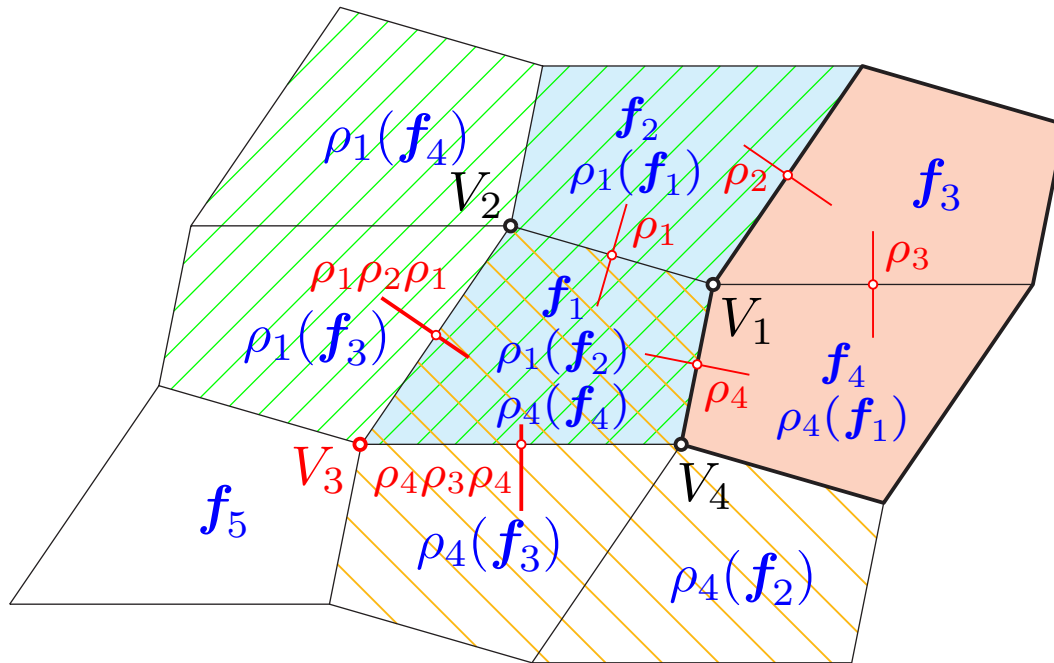
$\rho_1$  maps the pyramid with vertex  $V_1$  onto the pyramid with vertex  $V_2$ .

$\rho_4$  maps the pyramid with vertex  $V_1$  onto the pyramid with vertex  $V_4$ .

There are two possibilities to continue the flexion onto the fourth pyramid with vertex  $V_3$ .



## 2. Kokotsakis' flexible tessellation

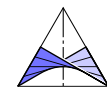


$\rho_1 \circ \rho_2 \circ \rho_1$  maps the pyramid with vertex  $V_2$  onto the pyramid with vertex  $V_3$ .

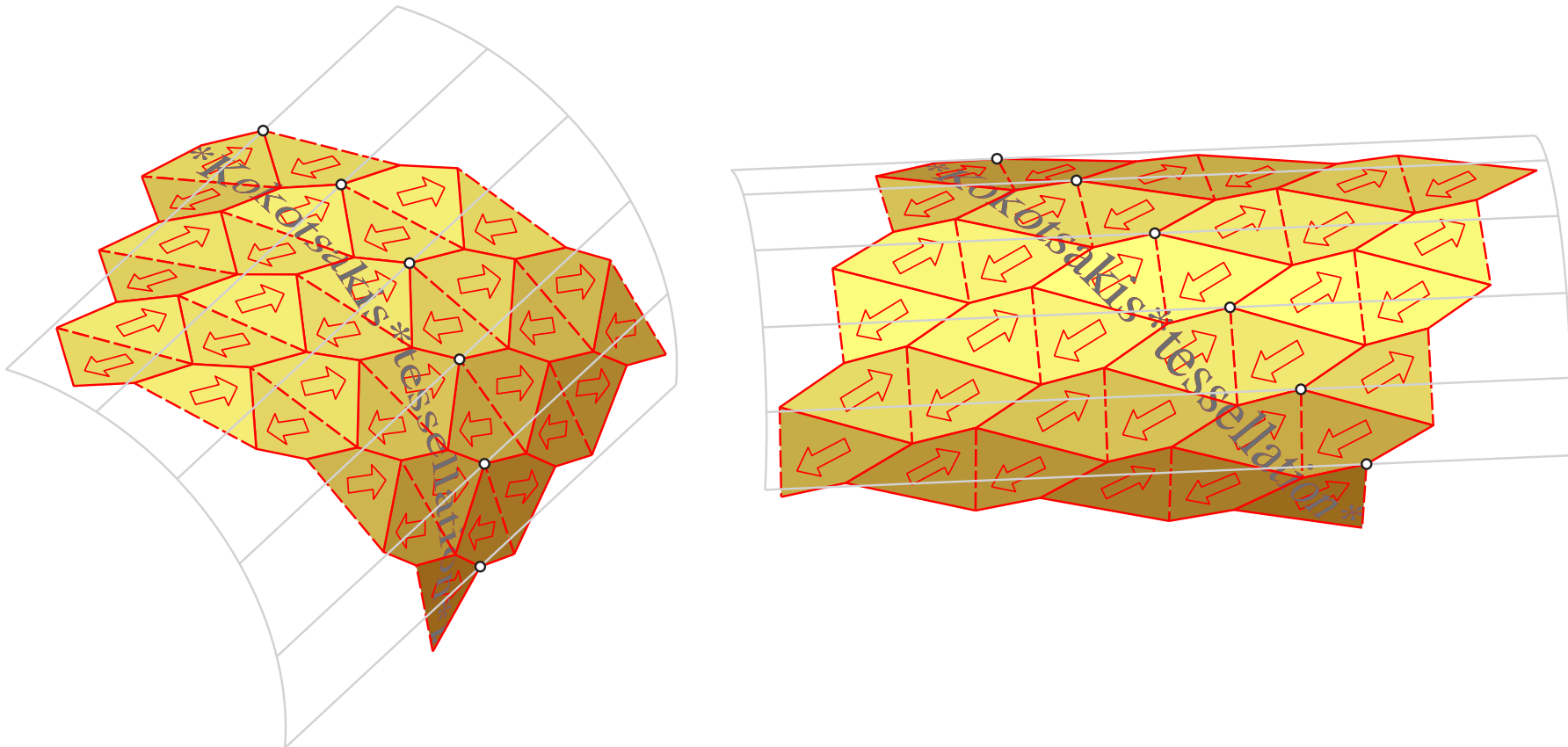
$\rho_4 \circ \rho_3 \circ \rho_4$  maps the pyramid with vertex  $V_4$  onto the pyramid with vertex  $V_3$ .

$f_5$  is the image of  $f_2 = \rho_1(f_1)$  under  $\rho_1 \circ \rho_2 \circ \rho_1$ , and image of  $f_4 = \rho_4(f_1)$  under  $\rho_4 \circ \rho_3 \circ \rho_4$ , as  $f_5 = \rho_1 \circ \rho_2(f_1) = \rho_4 \circ \rho_3(f_1)$ .

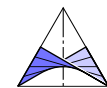
The complete pose arises from the “hexagon”  $f_3 \cup f_4$  under iterations of the helical motions  $r = \rho_2 \circ \rho_1$  and  $l = \rho_4 \circ \rho_1$ . This can be continued to a  $m \times n$  mesh.



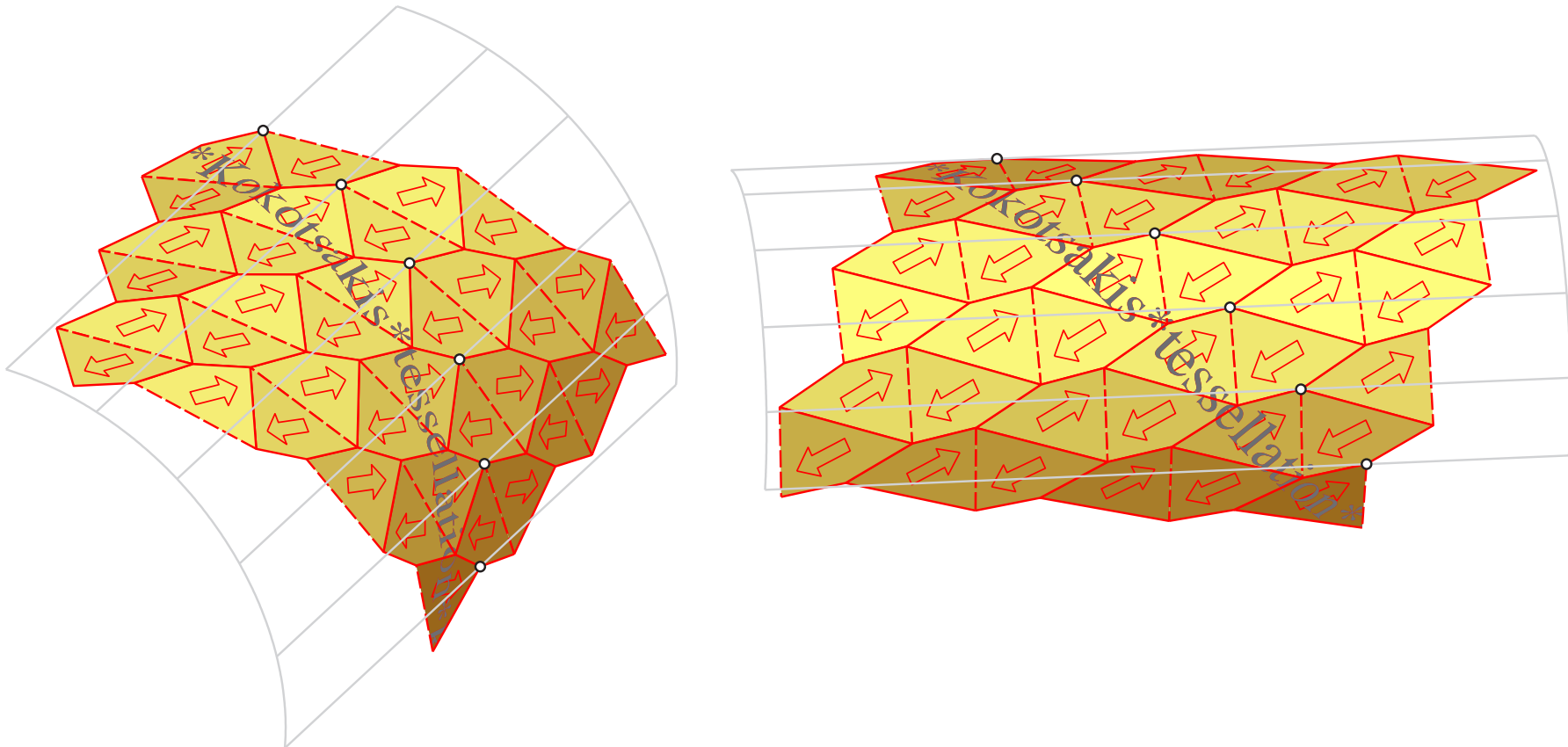
## 2. Kokotsakis' flexible tessellation



At each flexion obtainable by a continuous self-motion of an  $m \times n$  tessellation mesh **all vertices** are located on a **right circular cylinder** (discrete conjugate quadrangular net on this cylinder)

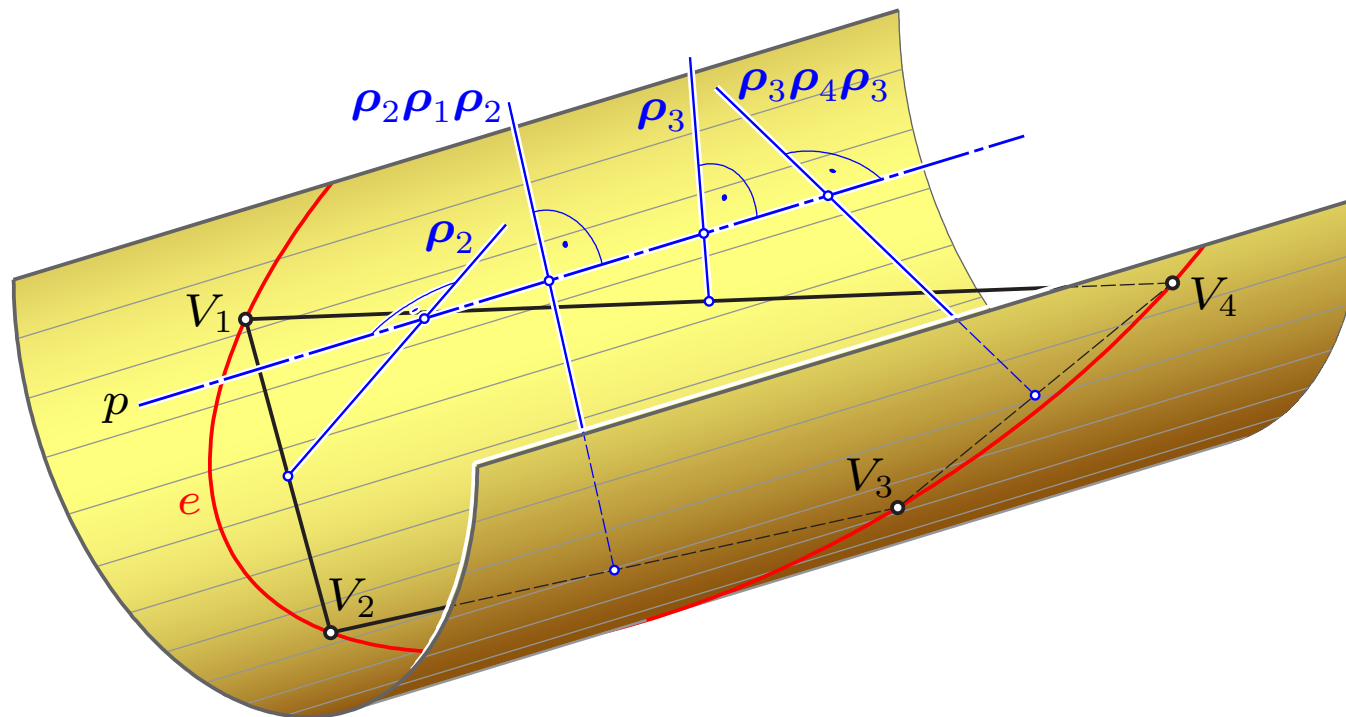


## 2. Kokotsakis' flexible tessellation

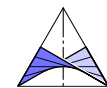


Each flexion of an  $\infty \times \infty$  tessellation mesh is periodic. Generically, its group of isomorphisms is generated by coaxial helical motions  $l, r$  and by  $\rho_4$ . It is isomorphic to that of the flat case (**p2**).

## 2. Kokotsakis' flexible tessellation

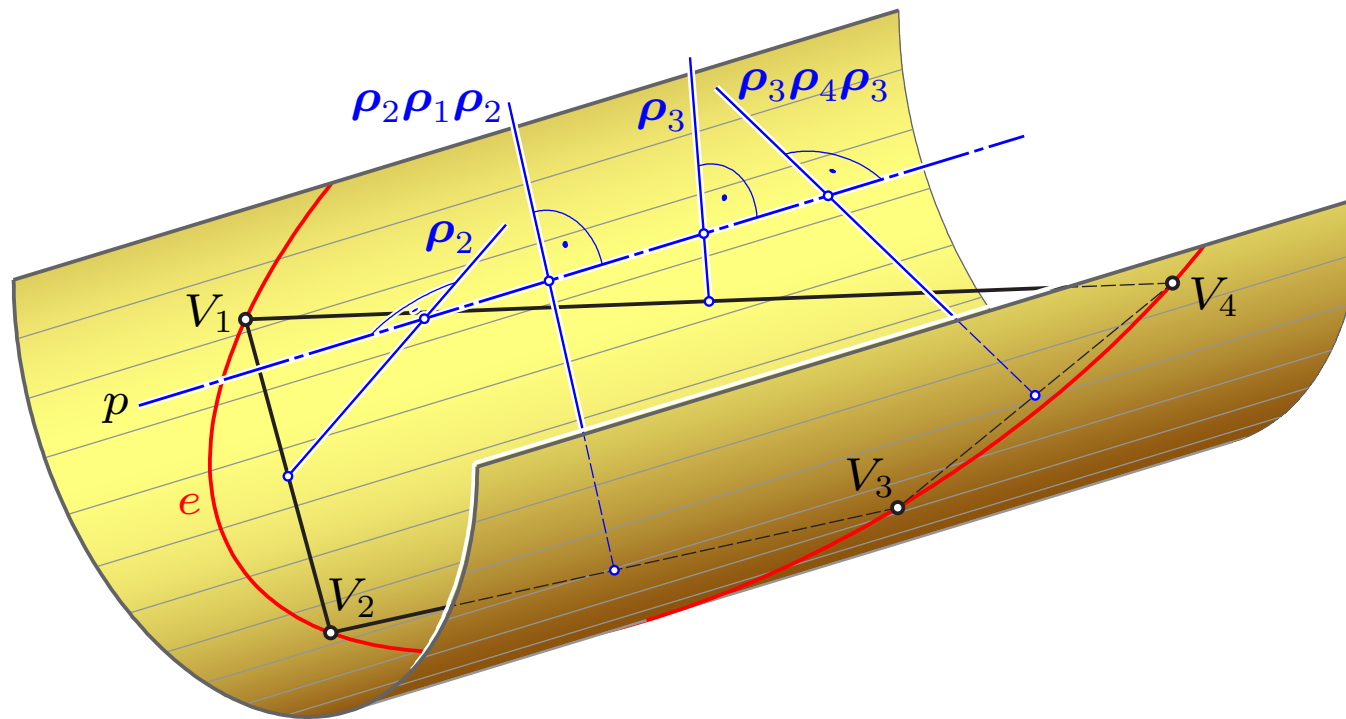


Another method to obtain the flexions: The plane spanned by  $f_{11}$  intersects the circumcylinder along an ellipse  $e$ .

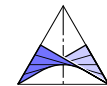




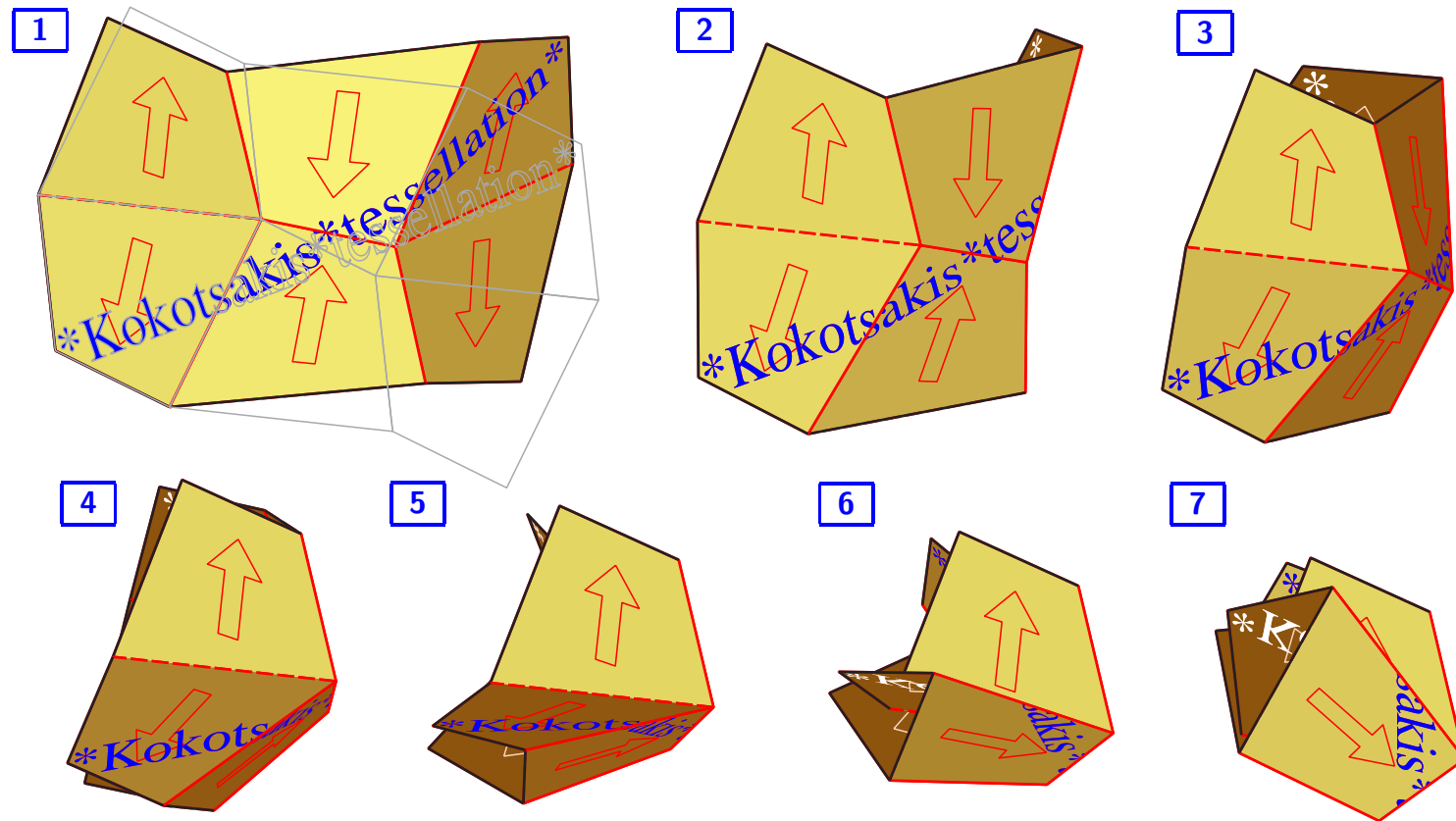
## 2. Kokotsakis' flexible tessellation



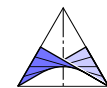
Conversely, there is a **one-parameter set of ellipses** passing through a given convex quadrangle. For each ellipse there are two cylinders of revolution passing through. Each such cylinder defines a flexion of a tessellation mesh (TM).



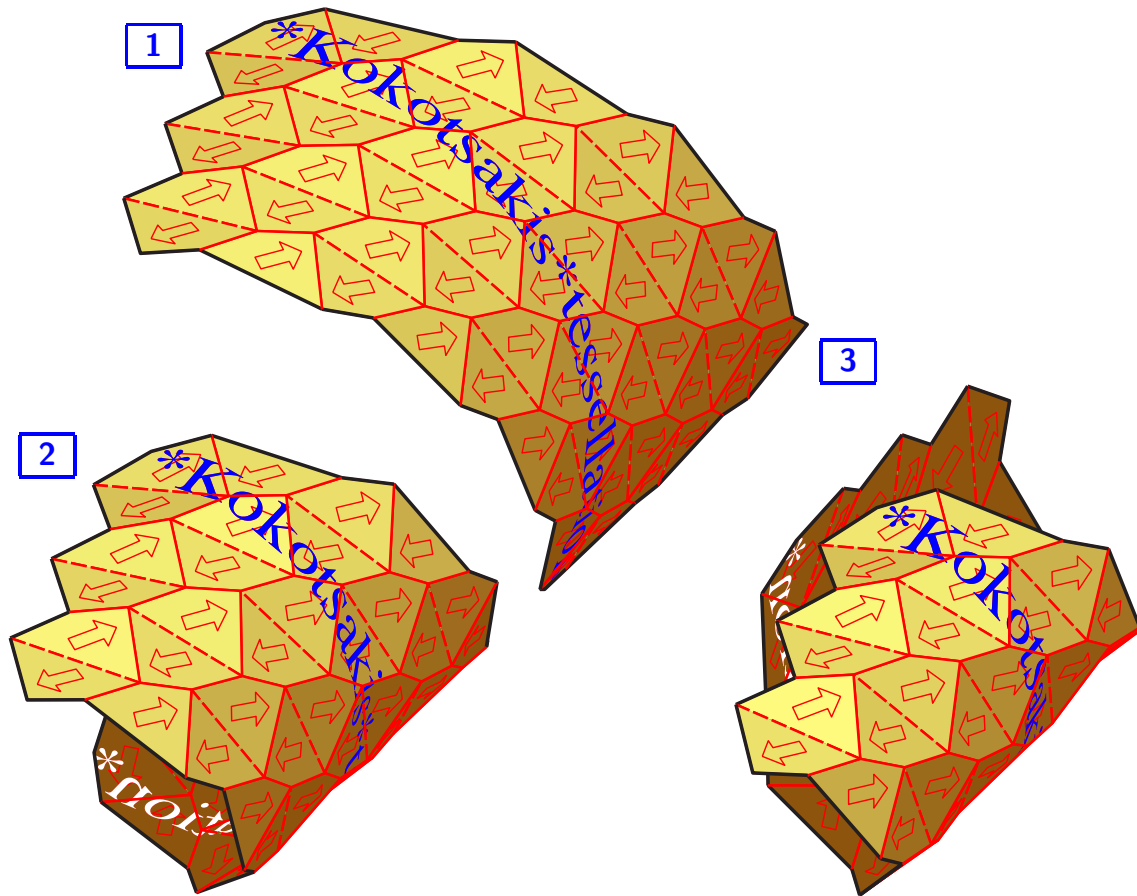
## 2. Kokotsakis' flexible tessellation



For quadrangles with circumcircle the mesh (= Voss surface) admits a **second flat pose** with coinciding circumcircles coincide (not free of self-intersections!)



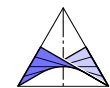
### 3. Flexion which tiles the cylinder



Left: Flexions of a  $9 \times 6$  TM

Under which conditions the flexion is *horizontally closing*, i.e., the right border zig-zag fits exactly to the left border — apart from a vertical shift?

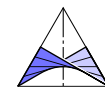
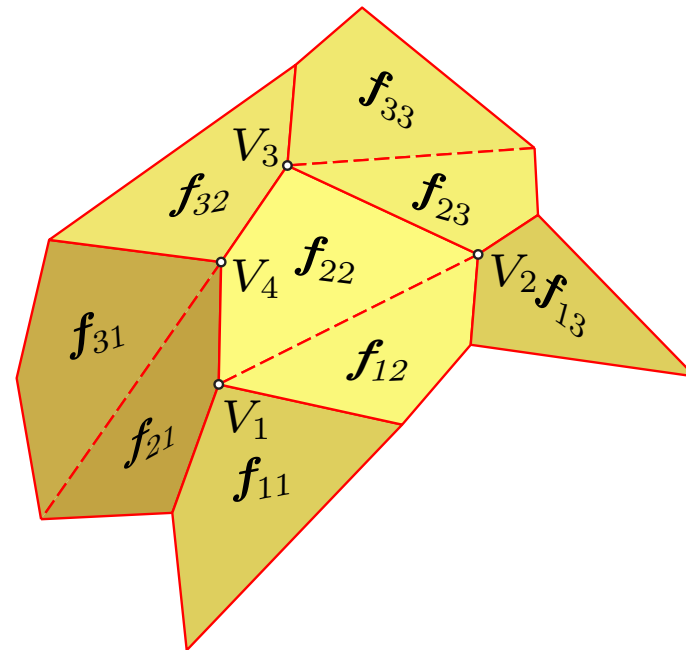
(the trapezoidal case with aligned borders is excluded)



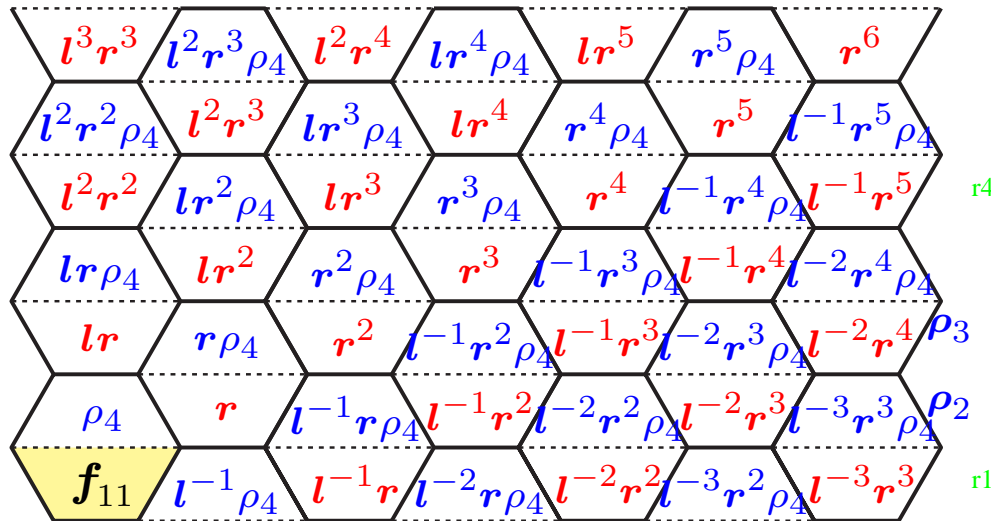
### 3. Flexion which tiles the cylinder

A  $m \times n$  **tessellation mesh** is a grid of  $m \times n$  quadrangles denoted by  $f_{ij}$ ,  $1 \leq i \leq m$ ,  $1 \leq j \leq n$

$$\begin{array}{ccccccc} f_{m1} & f_{m2} & f_{m3} & \cdots & f_{mn} & & \\ \vdots & \vdots & \vdots & & \vdots & & \\ f_{21} & f_{22} & f_{23} & \cdots & f_{2n} & & \\ f_{11} & f_{12} & f_{13} & \cdots & f_{1n} & & \end{array}$$



### 3. Flexion which tiles the cylinder



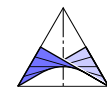
This scheme of a  $7 \times 7$  TM shows which product of  $l$ ,  $r$  and  $\rho_4$  must be applied to  $f_{11}$  to obtain  $f_{ij}$ .

Each flexion of an  $\infty \times \infty$  TM is **periodic**; the group of isomorphism acts transitively on the quadrangles.

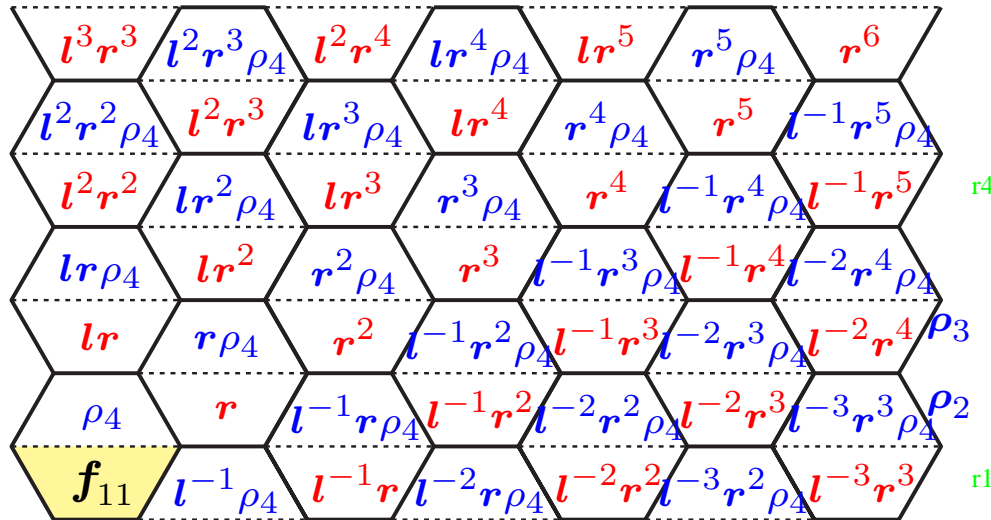
**Lemma:**  $f_{11}$  can be transformed into  $f_{ij}$  according to

$$f_{ij} = \begin{cases} l^{\frac{i-j}{2}} r^{\frac{i+j}{2}-1}(f_{11}) & \text{for } i+j \equiv 0 \pmod{2}, \\ l^{\frac{i-j-1}{2}} r^{\frac{i+j-3}{2}} \rho_4(f_{11}) & \text{for } i+j \equiv 1 \pmod{2}. \end{cases}$$

$$(r = \rho_2 \circ \rho_1 \text{ and } l = \rho_4 \circ \rho_1)$$



### 3. Flexion which tiles the cylinder



For odd  $m$   $f_{2n+1} = r(f_{1n})$  is identical with  $f_{k+2,1}$  of the most-left row,  $k \equiv 1 \pmod{2}$ , iff

$$l^{\frac{1-n}{2}} r^{\frac{n+1}{2}} = l^{\frac{k+1}{2}} r^{\frac{k+1}{2}} d(2\pi)$$

Since the involved helical motions commute pairwise, we obtain

$$l^{-\frac{n+k}{2}} \circ r^{\frac{n-k}{2}} = d(2\pi).$$

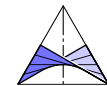
#### Theorem:

A flexion of an  $m \times n$  TM closes horizontally with vertical shift  $k$

$\iff$

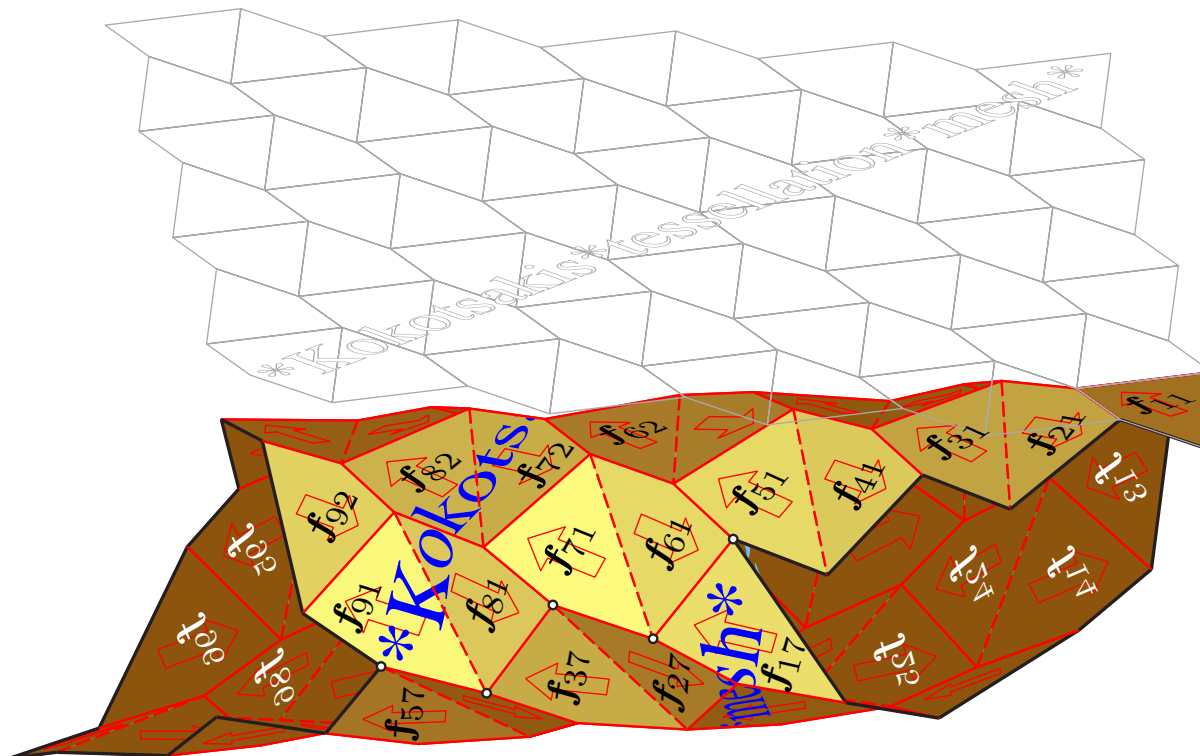
$$\exists a, b \in \mathbb{Z} : l^a r^b = d(2\pi).$$

$$n = -a + b, \text{ shift } k = -a - b.$$



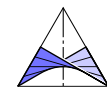
### 3. Flexion which tiles the cylinder

Example: Horizontally closing  $7 \times 9$  TM satisfying  $l^{-6}r = d(2\pi)$ :



How to obtain a closing version ?

- Either numerically by minimizing a certain distance.
- Or by starting with two coaxial helical motions  $r, l$  obeying  $l^a r^b = d(2\pi)$  and  $\rho_4$ .



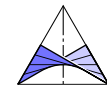
### 3. Flexion which tiles the cylinder

After specifying  $\rho_1, \rho_2, \rho_4$  and any first vertex  $V_1$  a quadrangle  $V_1 \dots V_4$  is defined. However, this will **not be planar**.

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**Lemma:**

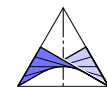
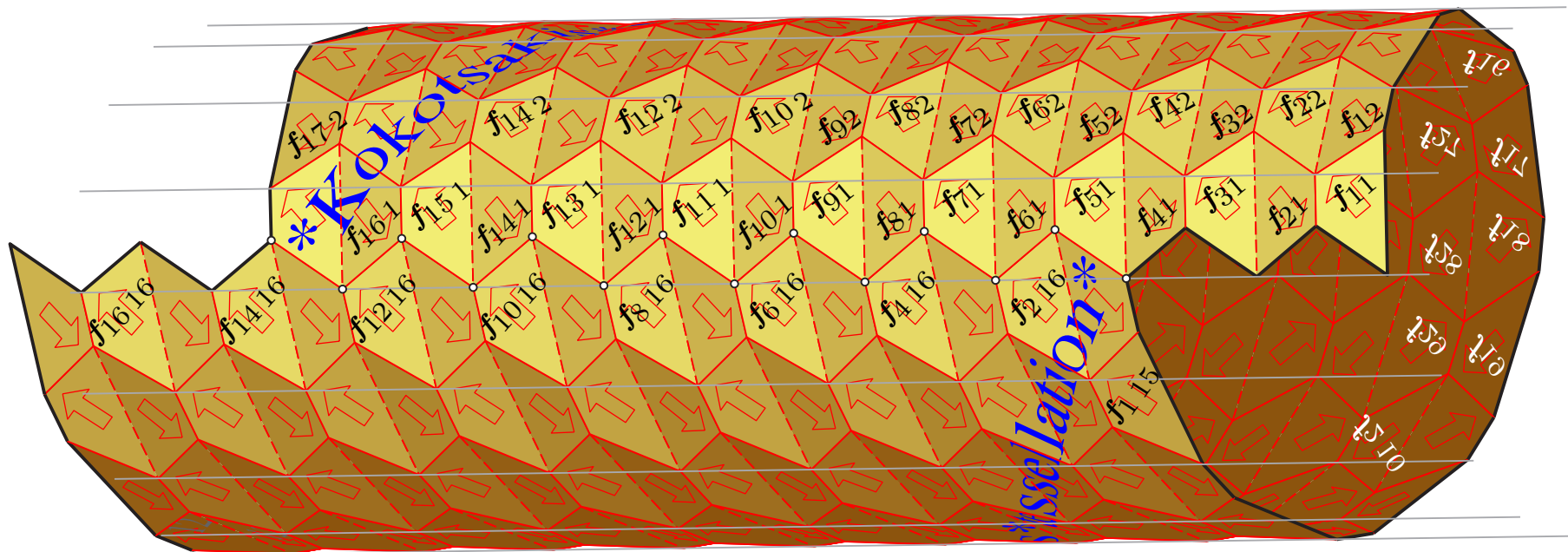
For planarity of the quadrangle  $V_1 \dots V_4$  it is necessary and sufficient to specify  $V_1$  on a **ruled surface of degree 3**.





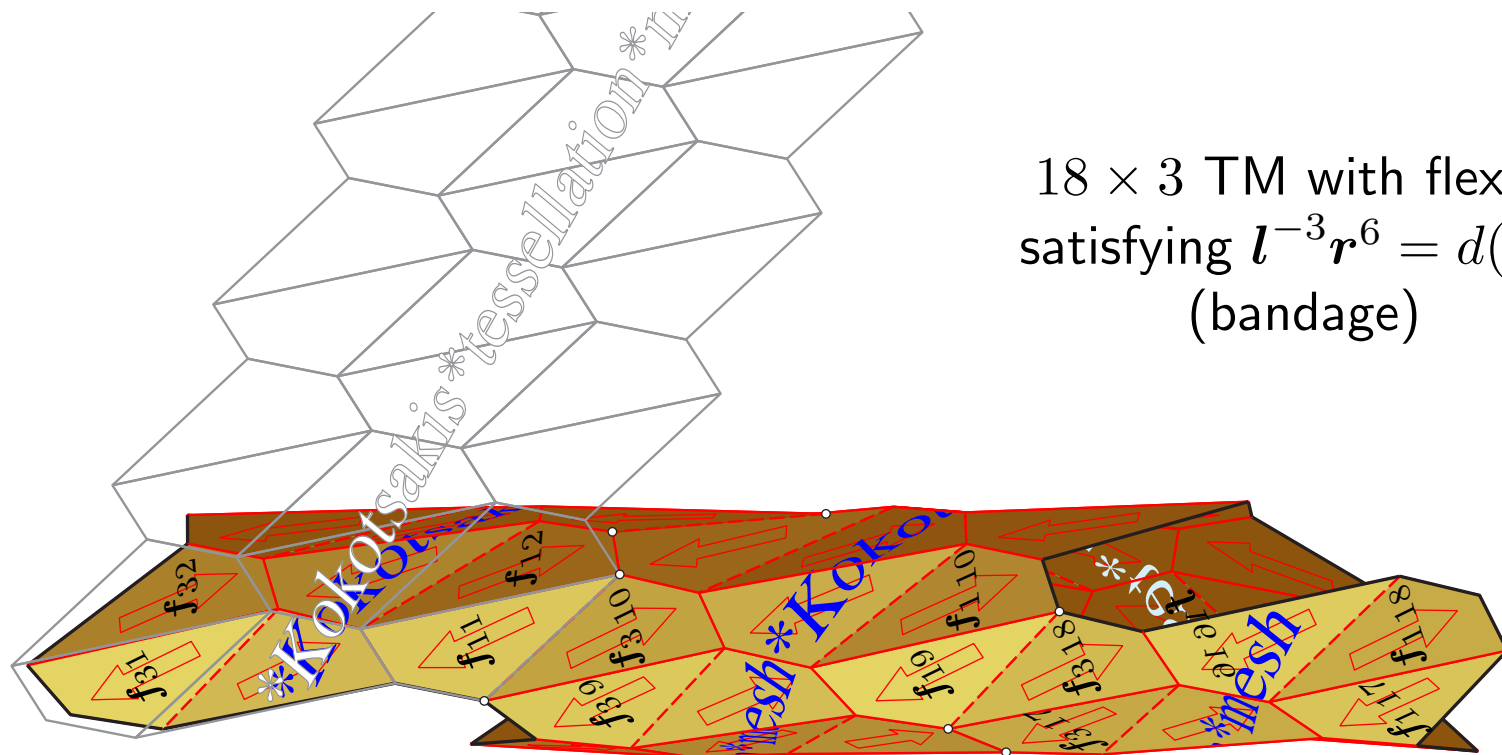
### 3. Flexion which tiles the cylinder

A basic trapezoid yields as nontrivial closing flexion of a  $16 \times 17$  TM a modified *Schwarz lantern* satisfying  $l^{-10}r^6 = d_{2\pi}$  and  $k = 4$ .

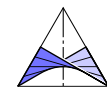


### 3. Flexion which tiles the cylinder

**Theorem:** For given axes of the  $180^\circ$ -rotations  $\rho_1, \rho_2, \rho_4$  there is a two-parameter set of planar convex quadrangles for tiling a cylinder.



$18 \times 3$  TM with flexion  
satisfying  $l^{-3}r^6 = d(2\pi)$   
(bandage)



# Rigidity of a quadrangular cylinder tiling

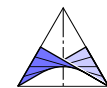
## Theorem:

When at a horizontally closing flexion of an  $m \times n$  TM the right and the left border line are glued together — at least at one vertex — then in the case of a non-cyclic base quadrangle the resulting quad mesh is infinitesimally rigid.

*Remark:* For a cyclic quadrangle  $V_1 \dots V_4$  the closing pose is flat. But this is trivially infinitesimally flexible.

*Proof:* We keep  $f_{11}$  fixed and assume that  $f_{1-k \ m+1}$  coincides with  $f_{11}$ . We will confirm that there is no non-trivial infinitesimal motion of the mesh such that any vertex of  $f_{1-k \ 1+m}$  obtains a zero-velocity.

We parametrize the self-motion of the TM by any parameter  $u$ .



# Rigidity of a quadrangular cylinder tiling

For all  $u \in I$  there is a **helical motion** about an axis  $p(u)$  through angle  $\varphi(u)$  and with translational length  $l(u)$  with  $f_{11} \mapsto f_{1-k} m_{+1}$ .

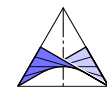
In a coordinate frame attached to  $f_{11}$  let  $p(u)$  be the unit vector of the axis  $p(u)$  and  $m(u)$  the position vector of the intersection between  $p(u)$  and  $[f_{11}]$ .

The **director cone** of the surface of axes is quadratic; we may assume  $\dot{p} \neq 0$  due to a regular parametrization of this cone.

The points  $m(u)$  are located on the **nine-point-conic** of the quadrangle  $f_{11}$ ; hence  $m(u)$  can never coincide with any vertex.

We set up the helical motion mapping  $x \in f_{11}$  onto  $x' \in f_{1-k} m_{+1}$  by

$$x' - m = \cos \varphi (x - m) + [(1 - \cos \varphi)(p \cdot (x - m)) + l] p + \sin \varphi [p \times (x - m)].$$



# Rigidity of a quadrangular cylinder tiling

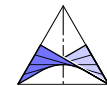
Differentiation by  $u$  yields for the infinitesimal motion of  $f_{1-k 1+m}$

$$\begin{aligned} \dot{\mathbf{x}}' - \dot{\mathbf{m}} = & -\dot{\varphi} \sin \varphi (\mathbf{x} - \mathbf{m}) - \cos \varphi \dot{\mathbf{m}} + [\dot{\varphi} \sin \varphi (\mathbf{p} \cdot (\mathbf{x} - \mathbf{m})) \\ & + (1 - \cos \varphi) (\dot{\mathbf{p}} \cdot (\mathbf{x} - \mathbf{m})) - (1 - \cos \varphi) (\mathbf{p} \cdot \dot{\mathbf{m}}) + \dot{l}] \mathbf{p} \\ & + [(1 - \cos \varphi) (\mathbf{p} \cdot (\mathbf{x} - \mathbf{m})) + l] \dot{\mathbf{p}} + \dot{\varphi} \cos \varphi [\mathbf{p} \times (\mathbf{x} - \mathbf{m})] \\ & + \sin \varphi [(\dot{\mathbf{p}} \times (\mathbf{x} - \mathbf{m})) - (\mathbf{p} \times \dot{\mathbf{m}})]. \end{aligned}$$

In the horizontally closing pose  $u = u_0$  with  $\varphi(u_0) = 2\pi$  and  $l(u_0) = 0$  remains:

$$\dot{\mathbf{x}}' = \mathbf{v}_{\mathbf{x}'} = \dot{l} \mathbf{p} + \dot{\varphi} [\mathbf{p} \times (\mathbf{x} - \mathbf{m})].$$

$\implies$  also the instantaneous motion of  $f_{1-k 1+m}$  is a helical motion about  $p(u_0)$  with angular velocity  $\dot{\varphi}(u_0)$  and translational velocity  $\dot{l}(u_0)$ .



## Rigidity of a quadrangular cylinder tiling

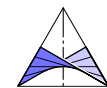
In the rotational case  $\dot{l} = 0$ ,  $\dot{\varphi} \neq 0$  point  $m$  would be fixed, but  $m$  never coincides with one vertex of  $f_{1-k, 1+m}$ .

Only under  $\dot{\varphi} = \dot{l} = 0$  there exists a fixed vertex; the complete face  $f_{1-k, 1+m}$  has a stillstand. However,  $\dot{l} = 0$  for  $u = u_0$  will lead to a contradiction.

---

Let  $(\tau, t)$  and  $(\sigma, s)$  denote the angles of rotation and lengths of translation of the helical motions  $l(u)$  and  $r(u)$ , respectively. The horizontally closing implies

$$a, b \in \mathbb{Z} \setminus \{(0, 0)\} \quad \text{with} \quad \varphi(u) = a\tau + b\sigma, \quad l(u) = at + bs.$$



## Rigidity of a quadrangular cylinder tiling

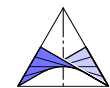
From  $l: v_1 \mapsto v_3$  and  $r: v_2 \mapsto v_4$  with  $v_1, \dots, v_4$  as vertices of  $f_{11}$  we obtain

$$s(u) = (v_3 - v_1) \cdot p(u), \quad t(u) = (v_4 - v_2) \cdot p(u).$$

$\implies \dot{l} = a\dot{t} + b\dot{s}$ . Hence,  $l = \dot{l} = 0$  for  $u = u_0$  results in

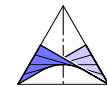
$$\mathbf{n} \cdot p(u_0) = \mathbf{n} \cdot \dot{p}(u_0) = 0 \quad \text{for } \mathbf{n} := a(v_4 - v_2) + b(v_3 - v_1) \neq \mathbf{0}.$$

The linearly independent vectors  $p(u_0)$  and  $\dot{p}(u_0)$  span a **tangent plane** of the quadratic director cone, and this plane is orthogonal to the vector  $\mathbf{n}$  which — as a linear combination of the two diagonal vectors of  $f_{11}$  — lies in a symmetry plane of the cone. Hence for a non-degenerate cone, i.e., for a non-cyclic base quadrangle,  $p(u_0)$  must be a direction vector of one of the generators in the symmetry plane parallel  $[f_{11}]$ . But these generators are no more axes of cylinders of rotation through the base quadrangle.  $\square$



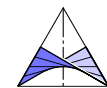
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