

# The Development of the Oloid

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**Abstract.** Let two unit circles  $k_A, k_B$  in perpendicular planes be given such that each circle contains the center of the other. Then the convex hull of these circles is called *Oloid*. In the following some geometric properties of the Oloid are treated analytically. It is proved that the development of the bounding torse  $\Psi$  leads to elementary functions only. Therefore it is possible to express the rolling of the Oloid on a fixed tangent plane  $\tau$  explicitly. Under this staggering motion, which is related to the well-known spatial Turbula-motion, also an ellipsoid  $\Phi$  of revolution inscribed in the Oloid is rolling on  $\tau$ . We give parameter equations of the curve of contact in  $\tau$  as well as of its counterpart on  $\Phi$ .

The surface area of the Oloid is proved to equal the area of the unit sphere. Also the volume of the Oloid is computed.

*Keywords:* Oloid, Turbula-motion, development of torsos.

*MSC 1994:* 51N05, 53A05, 53A17

## 1. Introduction

Let  $k_A, k_B$  be two unit circles in perpendicular planes  $\Pi_1, \Pi_2$  such that  $k_A$  passes through the center  $M_B$  of  $k_B$  and  $k_B$  passes through the center  $M_A$  of  $k_A$  (see Fig. 1)<sup>1</sup>. The *torse* (developable)  $\Psi$  connecting  $k_A$  and  $k_B$  is the enveloping surface of all planes  $\tau$  that touch  $k_A$  and  $k_B$  simultaneously. If any tangent plane  $\tau$  contacts  $k_A$  at  $A$  and  $k_B$  at  $B$ , then the line  $AB$  is a generator of  $\Psi$ . In this case the tangent line of  $k_A$  at  $A$  must intersect the tangent line of  $k_B$  at  $B$  in a finite or infinite point  $T$  on the line  $l_2$  of intersection between  $\Pi_1$  and  $\Pi_2$  (see Fig. 2; the triangle  $ABT$  can also be found in Fig. 5 and Fig. 6).

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<sup>1</sup>All figures in this paper are orthogonal views. But only in Fig. 5 and Fig. 6 the superscript “ $n$ ” is used to indicate that geometric objects have been projected orthogonally into a plane.

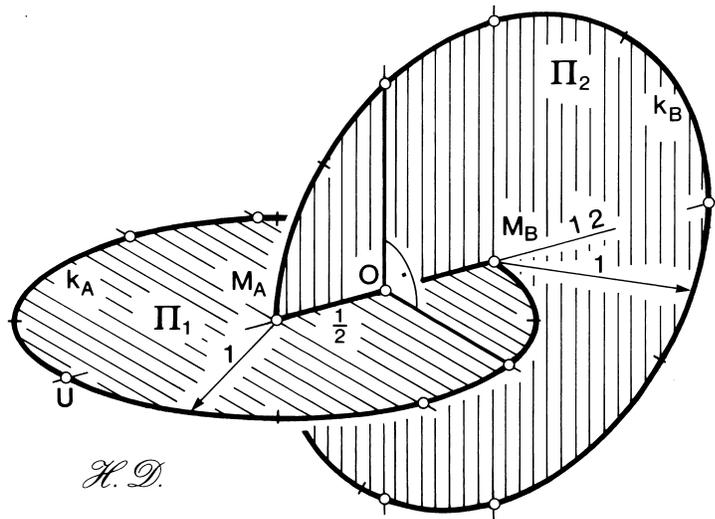


Figure 1: Circles  $k_A, k_B$  defining the Oloid

We choose the planes  $\Pi_1, \Pi_2$  as coordinate planes and the midpoint  $O$  of  $M_A M_B$  as the origin of a cartesian coordinate system. Then we may set up the equations of  $k_A, k_B$  as

$$\begin{aligned} k_A: x^2 + (y + \frac{1}{2})^2 &= 1 & \text{and} & & z &= 0 \\ k_B: (y - \frac{1}{2})^2 + z^2 &= 1 & \text{and} & & x &= 0. \end{aligned} \tag{1}$$

We parametrize the torse  $\Psi$  by the arc-length  $t$  of  $k_A$  with the starting point  $t = 0$  at  $U$  on

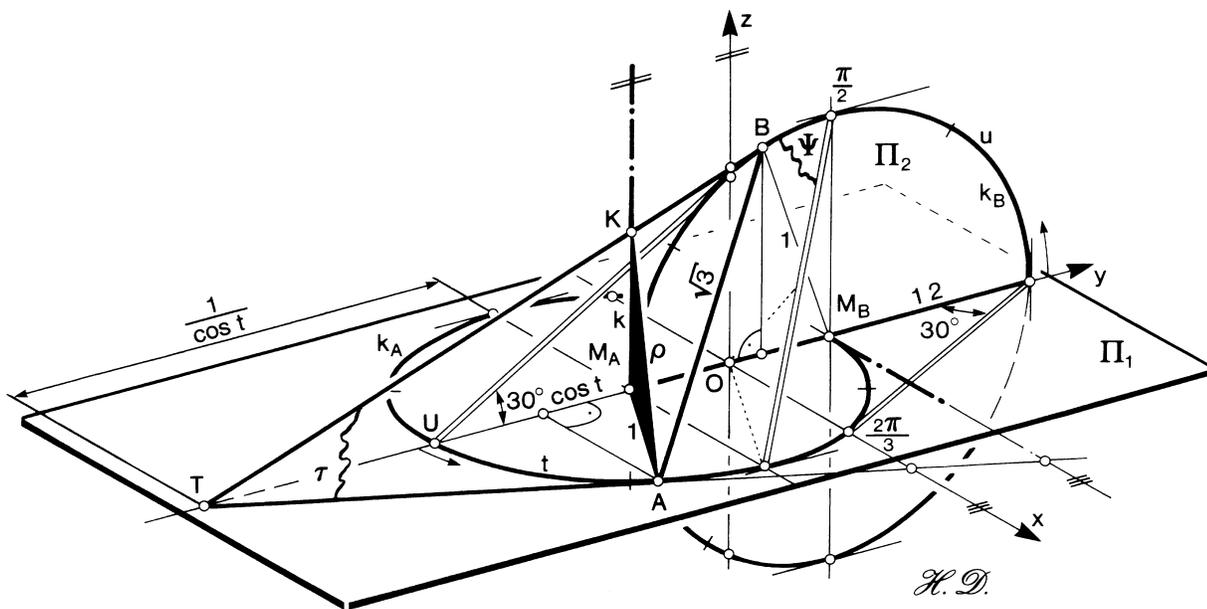


Figure 2: Coordinate system and notation

the negative  $y$ -axis. Then we obtain the coordinates

$$A = \left( \sin t, -\frac{1}{2} - \cos t, 0 \right). \tag{2}$$

Since the point  $T$  on the  $y$ -axis is conjugate to  $A$  with respect to  $k_A$ , we get

$$T = \left( 0, -\frac{2 + \cos t}{2 \cos t}, 0 \right). \quad (3)$$

In the same way conjugacy between  $T$  and  $B$  with respect to  $k_B$  implies

$$B = \left( 0, \frac{1}{2} - \frac{\cos t}{1 + \cos t}, \pm \frac{\sqrt{1 + 2 \cos t}}{1 + \cos t} \right). \quad (4)$$

The upper sign of the  $z$ -coordinate corresponds to the upper half of  $\Psi$ .<sup>2</sup>

From (2) and (4) we compute the squared length of the line segment  $AB$  as

$$\overline{AB}^2 = \sin^2 t + \left( 1 + \cos t - \frac{\cos t}{1 + \cos t} \right)^2 + \frac{1 + 2 \cos t}{(1 + \cos t)^2} = \sin^2 t + (1 + \cos t)^2 - 2 \cos t + 1,$$

which results in

**Theorem 1:** *All line segments  $AB$  of the torse  $\Psi$  are of equal length*

$$\overline{AB} = \sqrt{3}. \quad (5)$$

*This surprising result has already been proved in [7]. But probably also P. SCHATZ was aware of this result when he took out a patent for the Oloid (cf. [8]) in 1933 (see also [9], Figures 155, 156 and p. 122).*

Let  $u$  denote the arc-length of  $k_B$ , starting on the positive  $y$ -axis. Then  $A \in k_A$  and  $B \in k_B$  are points of the same generator of  $\Psi$  if and only if the parameters  $t$  of  $A$  and  $u$  of  $B$  obey the involutive relation

$$\cos u = -\frac{\cos t}{1 + \cos t} \quad \text{or} \quad \cos^2 \frac{t}{2} \cos^2 \frac{u}{2} = \frac{1}{4}. \quad (6)$$

For real generators of  $\Psi$  the condition  $1 + 2 \cos t \geq 0$  is necessary. By the restriction

$$-\frac{2\pi}{3} < t < \frac{2\pi}{3} \quad \text{and} \quad -\frac{2\pi}{3} < u < \frac{2\pi}{3} \quad (7)$$

we avoid vanishing denominators. It has to be noted that for  $\Psi$  the parametrization by  $t$  becomes singular at  $t = \pm 2\pi/3$ .

In the following we restrict each generator of  $\Psi$  to the line segment  $AB$ . Thus we obtain just the boundary of the *convex hull* of  $k_A$  and  $k_B$ .

## 2. Development of the Torse $\Psi$

When  $\Psi$  is developed into a plane  $\tau$ , then the circles  $k_A, k_B$  are isometrically transformed into planar curves  $k_A^d, k_B^d$ , respectively. It is well-known from Differential Geometry (see e.g. [11], p. 209 or [12], p. 72) that at corresponding points  $A \in k_A \subset \Psi$  and  $A^d \in k_A^d \subset \tau$  the geodesic curvatures are equal. This can be expressed in a more geometric way as follows (cf. [4], p. 295):

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<sup>2</sup>In the generalization presented in [5] the circles  $k_A, k_B$  are replaced by congruent ellipses with a common axis.

When  $\tau$  is specified as the tangent plane of  $\Psi$  along the generator  $AB$ , then the curvature center  $K$  of  $k_A^d$  at  $A^d = A$  is located on the curvature axis of  $k_A$  at  $A$ , which is the axis of revolution of (the curvature circle)  $k_A$  (see Fig. 2, compare Fig. 3). Since  $K = (-\frac{1}{2}, 0, \pm k)^3$  is aligned with  $T$  and  $B$ , we get for the squared curvature radius

$$\rho^2 = \overline{AK}^2 = 1 + k^2 = \frac{2 + 2 \cos t}{1 + 2 \cos t}.$$

Hence the curvature  $\kappa$  of  $k_A^d$  reads

$$\frac{1}{\rho} = \kappa(t) = \sqrt{\frac{1 + 2 \cos t}{2(1 + \cos t)}}. \quad (8)$$

This is the so-called natural equation of  $k_A^d$  with arc-length  $t$ .<sup>4</sup>

In order to deduce an explicit representation of  $k_A^d$ , we choose  $\tau$  as the tangent plane at the point  $U \in k_A$  with minimal  $y$ -coordinate. In  $\tau$  we introduce a cartesian coordinate system with origin  $U^d = U$  and axes  $I$  and  $II$  (see Fig. 3). We define the first coordinate-axis  $I$  parallel to the tangent vector of  $k_A$  at  $U$ . Then due to RICCATI's formula (see e.g. [10], p. 44) we get

$$\begin{aligned} I_A(t) &= I_0 + \int_0^t \cos \alpha(t) dt \\ II_A(t) &= II_0 + \int_0^t \sin \alpha(t) dt \end{aligned} \quad \text{for } \alpha(t) := \alpha_0 + \int_0^t \kappa(t) dt \quad (9)$$

with the specifications  $\alpha_0 = I_0 = II_0 = 0$ . By integration of (8) we obtain

$$\alpha(t) = 2 \arcsin \frac{\sqrt{6} \sin t}{3\sqrt{1 + \cos t}} - \arcsin \frac{\sqrt{3} \tan \frac{t}{2}}{3}. \quad (10)$$

**Theorem 2:** *In the cartesian coordinate system  $(I, II)$  (see Fig. 4) the arc length parametrization of the development  $k_A^d$  of the circle  $k_A$  reads*

$$\begin{aligned} I_A(t) &= \frac{2\sqrt{3}}{9} \left[ \sqrt{2(1 + 2 \cos t)(1 - \cos t)} + \arccos \frac{\sqrt{2} \cos t}{\sqrt{1 + \cos t}} \right] \\ II_A(t) &= \frac{\sqrt{3}}{9} \left[ 4(1 - \cos t) + \ln \frac{2}{1 + \cos t} \right]. \end{aligned} \quad (11)$$

*Proof:* The integrals in the left column of (9) could not be immediately solved with the use of common computer-algebra-systems. We succeeded as follows: The integral for  $II_A(t)$  can be transformed into

$$\begin{aligned} II_A(t) &= \int_0^t \sin \left( 2 \arcsin \frac{\sqrt{6} \sin t}{3\sqrt{1 + \cos t}} - \arcsin \frac{\sqrt{3} \tan \frac{t}{2}}{3} \right) dt = \\ &= \int_0^t \left[ \frac{4\sqrt{6} \sin \frac{t}{2} (1 + 2 \cos t)}{9 \sqrt{1 + \cos t}} - \frac{\sqrt{3} \tan \frac{t}{2} (4 \cos t - 1)}{9} \right] dt, \end{aligned}$$

<sup>3</sup>The sign of the  $z$ -coordinate is equal to that of  $B$  in (4).

<sup>4</sup>Note  $\dot{\rho}(0) = 0$ , but  $\ddot{\rho}(0) = \frac{1}{18}\sqrt{3} \neq 0$ . This proves that at  $U^d$  there is exactly a four-point contact between  $k_A^d$  and its curvature circle (see Fig. 4 or Fig. 5).

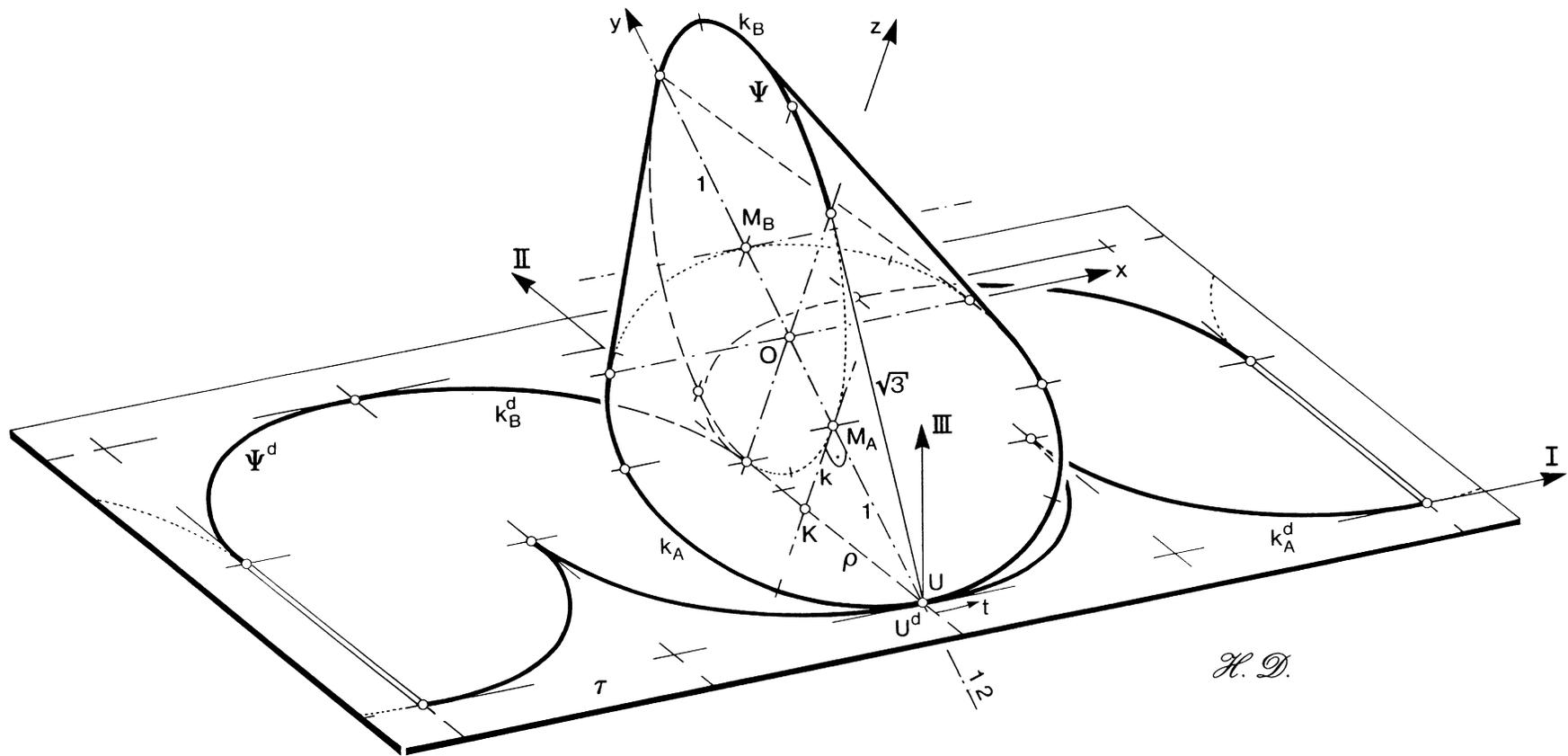


Figure 3: Axonometric view of the Oloid and its development into  $\tau$

and this gives rise to the second equation in (11). From

$$\frac{dII_A}{dt} = \frac{\sqrt{3}}{9} \sin t \left( 4 + \frac{1}{1 + \cos t} \right) = \sin \alpha \quad (12)$$

due to (9) we obtain

$$\frac{dI_A}{dt} = \cos \alpha = \sqrt{1 - \left( \frac{dII_A}{dt} \right)^2} = \frac{\sqrt{6}(1 + 2 \cos t)^{\frac{3}{2}}}{9\sqrt{1 + \cos t}}. \quad (13)$$

Then the integration can be carried out using the substitution  $\bar{t} := \tan \frac{t}{2}$ . The first quarter of the developed curve  $k_A^d$  ends at

$$(I_A(\frac{2\pi}{3}), II_A(\frac{2\pi}{3})) = \left( \frac{2\pi\sqrt{3}}{9}, \frac{2\sqrt{3}}{9}(3 + \ln 2) \right) \approx (1.2092, 1.4215). \quad \square$$

There is an analogous representation of the developed image  $k_B^d$  of the circle  $k_B$  in terms of its arc-length  $u$ . The curves  $k_A^d$  and  $k_B^d$  are congruent since halfturns about the axes  $x \pm z = y = 0$  interchange  $k_A$  and  $k_B$  while the Oloid is transformed into itself. However, based on (11) and due to (5) the curve  $k_B^d$  can also be parametrized in the form

$$\begin{aligned} I_B(t) &= I_A(t) + \sqrt{3} \cos e_{AB}, \\ II_B(t) &= II_A(t) + \sqrt{3} \sin e_{AB}. \end{aligned} \quad (14)$$

Here the angle  $e_{AB} = \alpha + \gamma$  (see Fig. 4) defines the direction of the developed generator  $A^d B^d$ . Angle  $\alpha$  has already been computed in (12) and (13).  $\gamma$  is the angle made by the generator  $AB$  of  $\Psi$  and the tangent vector

$$\mathbf{v}_A = (\cos t, \sin t, 0) \quad (15)$$

of  $k_A$  at  $A$ . The dot product of  $\mathbf{v}_A$  and the vector  $\overrightarrow{AB}$  according to (2) and (4) gives

$$\sqrt{3} \cos \gamma = \mathbf{v}_A \cdot \overrightarrow{AB} = -\sin t \cos t + \sin t + \sin t \cos t - \frac{\sin t \cos t}{1 + \cos t} = \frac{\sin t}{1 + \cos t}.$$

Elementary trigonometry leads to

$$\sin \gamma = \sqrt{\frac{2(1 + 2 \cos t)}{3(1 + \cos t)}} \quad (16)$$

and finally to

$$\begin{aligned} \sin e_{AB} &= \frac{7 + 7 \cos t + 4 \cos^2 t}{9(1 + \cos t)} \\ \cos e_{AB} &= -\frac{2\sqrt{2}(2 + \cos t)\sqrt{(1 - \cos t)(1 + 2 \cos t)}}{9(1 + \cos t)}. \end{aligned} \quad (17)$$

We substitute these formulas in (14). Then due to (11) we obtain





of  $e_{k_A^d}$  makes use of the curvature radius  $\rho$  according to (8). From (12) and (13) we obtain

$$\begin{aligned}\rho \sin \alpha &= \frac{(5 + 4 \cos t) \sqrt{6(1 - \cos t)}}{9\sqrt{1 + 2 \cos t}} \\ \rho \cos \alpha &= \frac{2\sqrt{3}}{9} (1 + 2 \cos t)\end{aligned}$$

and finally as parametrization of the evolute  $e_{k_A^d}$  of  $k_A^d$

$$\begin{aligned}I_K(t) &= \frac{2\sqrt{3}}{9} \arccos \frac{\sqrt{2} \cos t}{\sqrt{1 + \cos t}} - \frac{\sqrt{2(1 - \cos t)}}{\sqrt{3(1 + 2 \cos t)}} \\ II_K(t) &= \frac{\sqrt{3}}{9} \left[ 6 + \ln \frac{2}{1 + \cos t} \right].\end{aligned}\tag{19}$$

The evolute  $e_{k_A^d}$  obviously (see Fig. 4) does not pass through the cusps of  $k_A^d$ ; the curvature radius  $\rho$  tends to infinity. This reveals that these cuspidal points are not ordinary. For  $k_B^d$  the TAYLOR-series expansion of the parameter representation (18) at  $t = 0$  is

$$I_B(t) = \frac{1}{360} t^5 + O(t^7), \quad II_B(t) = \sqrt{3} + \frac{\sqrt{3}}{12} t^2 + O(t^4).$$

Therefore the singularities of  $k_A^d$  and  $k_B^d$  are of order 2 and class 3 (German: Rückkehrflachpunkte).

### 3. Motions Related to the Oloid

According to Fig. 3 we assume that the Oloid is rolling on the upper side of  $\tau$ . In the following we therefore choose for point  $B$  in (4) the negative  $z$ -coordinate. For the sake of brevity we substitute

$$s := \sin t \quad \text{and} \quad c := \cos t \quad \text{with} \quad -\frac{1}{2} < c \leq 1, \quad -1 \leq s \leq 1, \quad s^2 + c^2 = 1.\tag{20}$$

In order to describe the rolling of  $\Psi$  on  $\tau$  we introduce a moving frame of  $\Psi$  with origin  $A \in k_A$ . The first vector of this frame is the tangent vector  $\mathbf{v}_A$  according to (15). The second vector  $\mathbf{w}_A$  perpendicular to  $\mathbf{v}_A$  is specified in the tangent plane  $\tau$ . We define

$$\mathbf{w}_A := \frac{1}{\sin \gamma} \left( \frac{1}{\sqrt{3}} \overrightarrow{AB} - \mathbf{v}_A \cos \gamma \right) = \frac{1}{\sqrt{2(1+c)}} \left( -s \sqrt{1+2c}, c \sqrt{1+2c}, -1 \right).\tag{21}$$

The vector

$$\mathbf{n}_A := \mathbf{v}_A \times \mathbf{w}_A = \frac{1}{\sqrt{2(1+c)}} \left( -s, c, \sqrt{1+2c} \right)\tag{22}$$

perpendicular to  $\tau$  completes this cartesian frame.  $\mathbf{n}_A$  is pointing to the interior of  $\Psi$ .

While the Oloid is rolling on the fixed plane  $\tau$ , the frame  $(A; \mathbf{v}_A, \mathbf{w}_A, \mathbf{n}_A)$  shall be moving along  $\Psi$  in such a way, that  $A$  is the running point of contact between  $k_A$  and  $\tau$ . This implies that  $A \in k_A$  is always coincident with the corresponding point  $A^d \in k_A^d$ . Therefore

the elements of the moving frame get the following coordinates with respect to the cartesian coordinate system  $(U^d; I, II, III)$  attached to  $\tau$ :

$$\begin{aligned} A &= (I_A(t), II_A(t), 0), & \mathbf{v}_A &= (\cos \alpha, \sin \alpha, 0), \\ \mathbf{w}_A &= (-\sin \alpha, \cos \alpha, 0), & \mathbf{n}_A &= (0, 0, 1). \end{aligned} \quad (23)$$

Let  $(x, y, z)$  denote the coordinates of any point  $P$  attached to the Oloid. The required representation of the motion consists of a matrix equation which allows to compute the instantaneous coordinates  $(I, II, III)$  of point  $P$  with respect to the fixed plane  $\tau$ , in dependence of the motion parameter  $t$ . In order to obtain this equation we firstly compute the coordinates  $(\xi, \eta, \zeta)$  of  $P$  with respect to the moving frame  $(A; \mathbf{v}_A, \mathbf{w}_A, \mathbf{n}_A)$ . Though  $P$  is attached to  $\Psi$ , these coordinates are dependent on  $t$ . From (2), (15), (21) and (22) we get

$$\begin{pmatrix} x \\ y \\ z \end{pmatrix} = \begin{pmatrix} s \\ -\frac{1}{2} - c \\ 0 \end{pmatrix} + \frac{1}{\sqrt{2(1+c)}} \begin{pmatrix} c\sqrt{2(1+c)} & -s\sqrt{1+2c} & -s \\ s\sqrt{2(1+c)} & c\sqrt{1+2c} & c \\ 0 & -1 & \sqrt{1+2c} \end{pmatrix} \begin{pmatrix} \xi \\ \eta \\ \zeta \end{pmatrix}. \quad (24)$$

Secondly, according to (23) the motion of the moving frame with respect to  $\tau$  (see Fig. 3) reads

$$\begin{pmatrix} I \\ II \\ III \end{pmatrix} = \begin{pmatrix} I_A(t) \\ II_A(t) \\ 0 \end{pmatrix} + \begin{pmatrix} \cos \alpha & -\sin \alpha & 0 \\ \sin \alpha & \cos \alpha & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} \xi \\ \eta \\ \zeta \end{pmatrix}.$$

Now we eliminate  $(\xi, \eta, \zeta)$  from these two matrix equations with orthogonal  $3 \times 3$ -matrices. After substituting (11), (12) and (13) we obtain by straight-forward calculation

**Theorem 4:** *Based on the cartesian coordinate systems  $(x, y, z)$  in the moving space and  $(I, II, III)$  in the fixed space, the rolling of the Oloid on the tangent plane  $\tau$  can be represented as*

$$\begin{pmatrix} I \\ II \\ III \end{pmatrix} = \frac{\sqrt{3}}{9} \begin{pmatrix} \frac{cs\sqrt{1+2c}}{2(1+c)\sqrt{2(1+c)}} + 2 \arccos \frac{c\sqrt{2}}{\sqrt{1+c}} \\ \frac{15+13c-c^2}{2(1+c)} + \ln \frac{2}{1+c} \\ \frac{3\sqrt{3}(2+c)}{2\sqrt{2(1+c)}} \end{pmatrix} + (a_{ij}) \begin{pmatrix} x \\ y \\ z \end{pmatrix}, \quad \text{where}$$

$$(a_{ij}) = \frac{\sqrt{3}}{9} \begin{pmatrix} \frac{(5+c)\sqrt{1+2c}}{\sqrt{2(1+c)}} & \frac{(2+c)s\sqrt{1+2c}}{(1+c)\sqrt{2(1+c)}} & \frac{(5+4c)s}{(1+c)\sqrt{2(1+c)}} \\ \frac{(c-1)s}{1+c} & \frac{5+5c-c^2}{1+c} & -\frac{(1+2c)\sqrt{1+2c}}{1+c} \\ -\frac{3s\sqrt{3}}{\sqrt{2(1+c)}} & \frac{3c\sqrt{3}}{\sqrt{2(1+c)}} & \frac{3\sqrt{3(1+2c)}}{\sqrt{2(1+c)}} \end{pmatrix}.$$

Here  $c$  and  $s$  stand for  $\cos t$  and  $\sin t$ , respectively, while the motion parameter  $t$  obeys (7).

The first vector on the right side of this matrix equation represents the path  $k_O$  of the Oloid's center  $O$  under this rolling motion. In particular, the third coordinate of this vector

gives the oriented distance

$$r := \frac{2+c}{2\sqrt{2(1+c)}} \quad (25)$$

between  $O$  and the tangent plane for each  $t$ . Due to the introduced moving frame, this distance  $r$  equals the dot product  $\mathbf{n}_A \cdot \overrightarrow{AO}$ . One can verify that for each  $t$  the velocity vector of the center curve  $k_O$  is perpendicular to the axis  $A^d B^d$  of the instantaneous rotation<sup>5</sup> (see orthogonal view  $k_O^n$  of  $k_O$  in Fig. 5 or Fig. 6).

The rolling of the Oloid is truly staggering. It is related to the Turbula motion (see [13] or [7]<sup>6</sup> and the references there) which is used for shaking liquids. It turns out that the Turbula motion is inverse to the motion of the moving frame in (24).

The circles  $k_A$  and  $k_B$  can also be seen as singular surfaces  $\widehat{k}_A, \widehat{k}_B$  of 2<sup>nd</sup> class. The coordinates  $(u_0 : u_1 : u_2 : u_3)$  of their tangent planes

$$u_0 + u_1 x + u_2 y + u_3 z = 0$$

match the “tangential equations”

$$\widehat{k}_A: 4u_0^2 - 4u_0 u_2 - 4u_1^2 - 3u_2^2 = 0, \quad \widehat{k}_B: 4u_0^2 + 4u_0 u_2 - 3u_1^2 - 4u_3^2 = 0.$$

Then due to a standard theorem of Projective Geometry the torse  $\Psi$  is not only tangent to  $k_A$  and  $k_B$  but to all surfaces of 2<sup>nd</sup> class included in the range which is spanned by  $\widehat{k}_A$  and  $\widehat{k}_B$ . Among these surfaces there is an ellipsoid  $\Phi$  of revolution<sup>7</sup> obeying the equation

$$\Phi: 6x^2 + 4y^2 + 6z^2 = 3 \quad \text{or} \quad \widehat{\Phi}: \frac{1}{2}(\widehat{k}_A + \widehat{k}_B) = 4u_0^2 - 2u_1^2 - 3u_2^2 - 2u_3^2 = 0 \quad (26)$$

with focal points  $M_A, M_B$  and semi-axes  $\frac{\sqrt{3}}{2}$  and  $\frac{1}{\sqrt{2}}$  (cf. [13], p. 31). The curve  $l$  of contact between  $\Phi$  and the torse  $\Psi$  is located on cylinders which are the images of  $k_A$  and  $k_B$ , respectively, in the polarity with respect to  $\Phi$ . Therefore this curve has the representations

$$l: 3x^2 + \left(y - \frac{1}{2}\right)^2 = 3z^2 + \left(y + \frac{1}{2}\right)^2 = 1 \quad \text{or} \\ x = \frac{s}{2+c}, \quad y = -\frac{3c}{2(2+c)}, \quad z = \frac{\pm\sqrt{1+2c}}{2+c}. \quad (27)$$

Together with the Oloid also the inscribed ellipsoid  $\Phi$  is rolling on  $\tau$ . In the fixed plane  $\tau$  the point of contact with the rolling ellipsoid traces a curve  $l^d$ . The parameter representation

$$l^d: I = \frac{2\sqrt{3}}{9} \arccos \frac{c\sqrt{2}}{\sqrt{1+c}}, \quad II = \frac{\sqrt{3}}{9} \left[ \ln \frac{2}{1+c} + \frac{3(5+c)}{2+c} \right], \quad III = 0 \quad (28)$$

of this isometric image of  $l \subset \Psi$  is obtained by transforming the coordinates of  $l$  given in (27) (negative sign) under the matrix equation of Theorem 4.

Fig. 6 shows not only the fixed tangent plane  $\tau$  with the developed curves  $k_A^d, k_B^d$  and  $l^d$  in true shape. In this figure also an orthogonal view of the Oloid with the inscribed ellipsoid  $\Phi$  and the curve  $l$  of tangency is displayed.

<sup>5</sup>In general the instantaneous motion is a helical motion. However when a torse is rolling on a plane, the helical parameter must vanish (cf. [3], p. 161 or [6]).

<sup>6</sup>In this paper a very particular plane-symmetric six-bar loop is studied which is also displayed in [1], Figure 1. In each position of this loop and for each two opposite links  $\Sigma, \Sigma'$  there is a plane  $\tau$  of symmetry. It turns out that relatively to  $\Sigma$  these planes  $\tau$  are tangent to a torse of type  $\Psi$ . The Turbula motion is the motion of  $\Sigma$  relative to  $\tau$ , when in  $\tau$  the generator of the torse is kept fixed.

<sup>7</sup>In the cases treated in [5]  $k_A$  and  $k_B$  are ellipses, but  $\Phi$  is a sphere. This implies that the center  $O$  of gravity has a constant distance to  $\tau$  during the rolling motion.

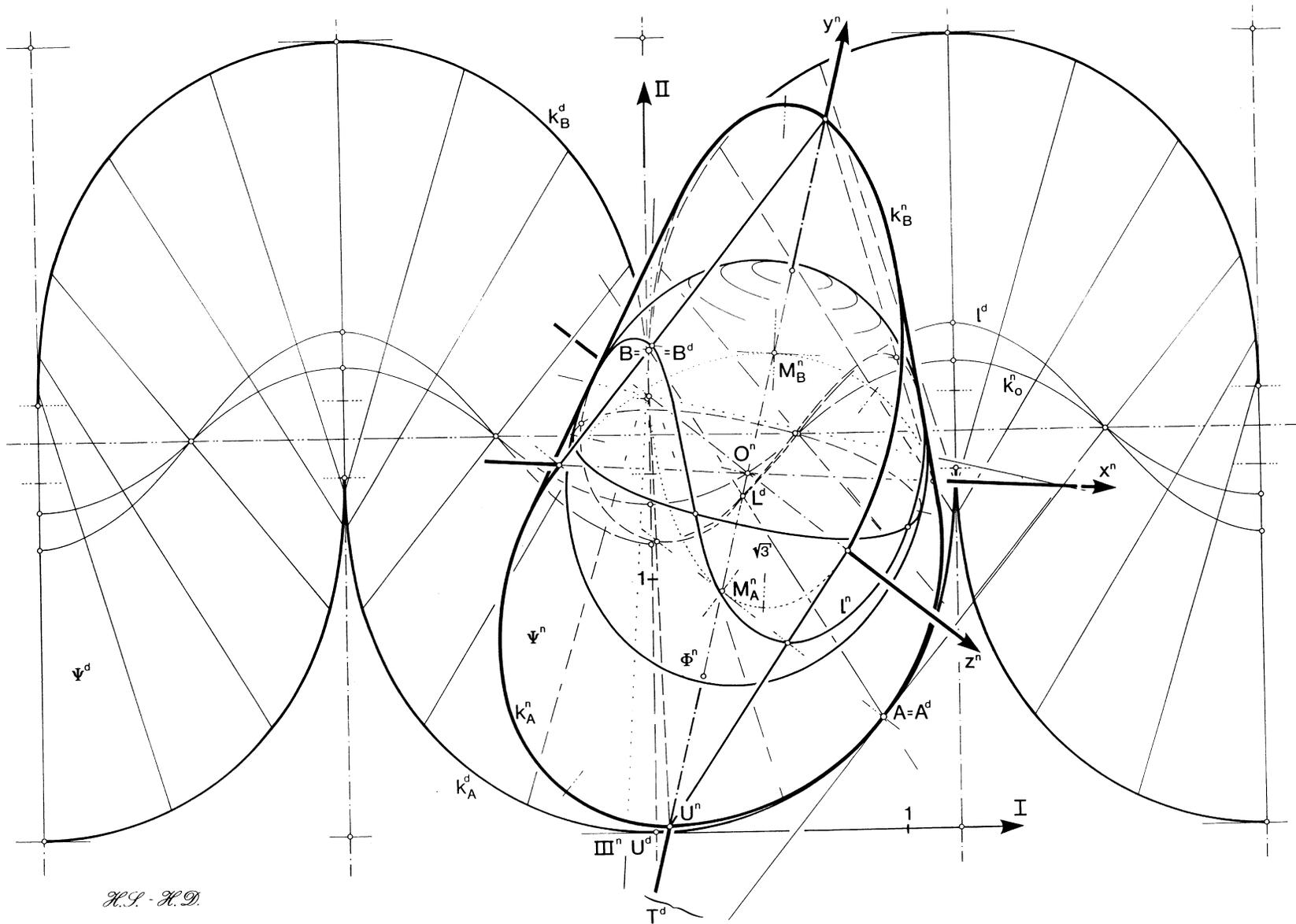


Figure 6: The Oloid and the inscribed ellipsoid  $\Phi$  are rolling on  $\tau$  while the curve  $l$  of contact between  $\Psi$  and  $\Phi$  traces  $l^d$

## 4. Surface Area and Volume of the Oloid

As the development of a torse is locally an isometry, the computation of the area of  $\Psi$  can be carried out either in the 3-space or after the development into the plane  $\tau$ . We prefer the latter and use a formula given in [2], p. 118, eq. (5): The area swept out by the line segment  $AB$  under a planar motion for  $t_0 \leq t \leq t_1$  can be computed according to

$$S = \int_{t_0}^{t_1} \left\| \frac{1}{2}(\mathbf{v}_A + \mathbf{v}_B) \times \overrightarrow{AB} \right\| dt, \quad (29)$$

where  $\mathbf{v}_A, \mathbf{v}_B$  are the velocity vectors of the endpoints. For vectors in  $\mathbb{R}^2$  the norm in this formula can be cancelled which gives rise to an even oriented area.

In the coordinate system  $(I, II)$  of  $\tau$  we obtain due to (14) and (11)

$$\begin{aligned} \overrightarrow{AB} &= (\sqrt{3} \cos e_{AB}, \sqrt{3} \sin e_{AB}), \quad \mathbf{v}_A = \left( \frac{dI_A}{dt}, \frac{dII_A}{dt} \right), \\ \mathbf{v}_B &= \left( \frac{dI_A}{dt} - \sqrt{3} \sin e_{AB} \frac{de_{AB}}{dt}, \frac{dII}{dt} + \sqrt{3} \cos e_{AB} \frac{de_{AB}}{dt} \right) \end{aligned}$$

and according to (12) and (13)

$$\frac{dS}{dt} = \sqrt{3} \left( \frac{dI_A}{dt} \sin e_{AB} - \frac{dII_A}{dt} \cos e_{AB} \right) - \frac{3}{2} \frac{de_{AB}}{dt} = \sqrt{3} \sin \gamma - \frac{3}{2} \frac{de_{AB}}{dt}.$$

Eq. (16) and the derivation of (17) lead to

$$\frac{dS}{dt} = \frac{\sqrt{2(1+2\cos t)}}{\sqrt{1+\cos t}} - \frac{3\sqrt{2} \cos t}{2\sqrt{(1+\cos t)(1+2\cos t)}}$$

which finally results in

$$\frac{dS}{dt} = \frac{2 + \cos t}{\sqrt{2(1 + \cos t)(1 + 2 \cos t)}}. \quad (30)$$

After integration we obtain up to a constant  $k$

$$S(t) = \frac{1}{2} \left[ \arcsin \frac{1 - 4 \cos t}{3} - \arcsin \frac{1 + 5 \cos t}{3(1 + \cos t)} \right] + k$$

and for the complete torse  $\Psi$

$$S_\Psi = 8 \left[ S \left( \frac{\pi}{2} \right) - S(0) \right] = 4 \left[ S \left( \frac{2\pi}{3} \right) - S(0) \right] = 4\pi. \quad (31)$$

**Theorem 5:** *The surface area of the Oloid equals that of the unit sphere.*

The computation of the Oloid's volume starts from (30): Each surface element of  $\Psi$  is the base of a volume element forming a pyramid with apex  $O$ . Its altitude  $r$  has already been computed in (25) as it equals the distance between  $O$  and the corresponding tangent plane. Thus we obtain

$$dV = \frac{r}{3} dS = \frac{(2 + \cos t)^2}{12(1 + \cos t)\sqrt{1 + 2 \cos t}} dt. \quad (32)$$

A numerical integration gives

$$V_\Psi = 8 \left[ V \left( \frac{\pi}{2} \right) - V(0) \right] \approx 3.05241. \quad (33)$$

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## References

- [1] J.E. BAKER: *The Single Screw Reciprocal to the General Plane-Symmetric Six-Screw Linkage*. JGG **1**, 5–12 (1997).
- [2] W. BLASCHKE, H.R. MÜLLER: *Ebene Kinematik*. Verlag von R. Oldenbourg, München 1956.
- [3] O. BOTTEMA, B. ROTH: *Theoretical Kinematics*. North-Holland Publ. Comp., Amsterdam 1979.
- [4] H. BRAUNER: *Lehrbuch der Konstruktiven Geometrie*. Springer-Verlag, Wien 1986.
- [5] C. ENGELHARDT, C. UCKE: *Zwei-Scheiben-Roller*. MNU, Math. Naturw. Unterr. **48**/5, 259–263 (1995).
- [6] M. HUSTY, A. KARGER, H. SACHS, W. STEINHILPER: *Kinematik und Robotik*. Springer, Berlin 1997.
- [7] S. KUNZE, H. STACHEL: *Über ein sechsgliedriges räumliches Getriebe*. Elem. Math. **29**, 25–32 (1974).
- [8] P. SCHATZ: Deutsches Reichspatent Nr. 589 452 (1933) in der allgemeinen Getriebe-klasse.
- [9] P. SCHATZ: *Rhythmusforschung und Technik*. Verlag Freies Geistesleben, Stuttgart 1975.
- [10] K. STRUBECKER: *Differentialgeometrie I*. 2. Aufl., Sammlung Göschen, Bd. 1113/1113a, Walter de Gruyter & Co, Berlin 1964.
- [11] K. STRUBECKER: *Differentialgeometrie II*. 2. Aufl., Sammlung Göschen, Bd. 1179/1179a, Walter de Gruyter & Co, Berlin 1969.
- [12] T.J. WILLMORE: *An Introduction to Differential Geometry*. Oxford University Press 1969.
- [13] W. WUNDERLICH: *Umwendung einer regelmäßigen sechsgliedrigen Würfelkette*. Proceedings IFToMM Symposium Mostar, May 1980, 23–33.

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